

Nd-Fe-B permanent magnets

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1. Introduction

Best permanent magnets known:

Based on either $\text{Nd}_2\text{Fe}_{14}\text{B}$ or SmCo_5

Important figures of merit

Magnetization M_s

- saturation magnetization

Coercivity H_C

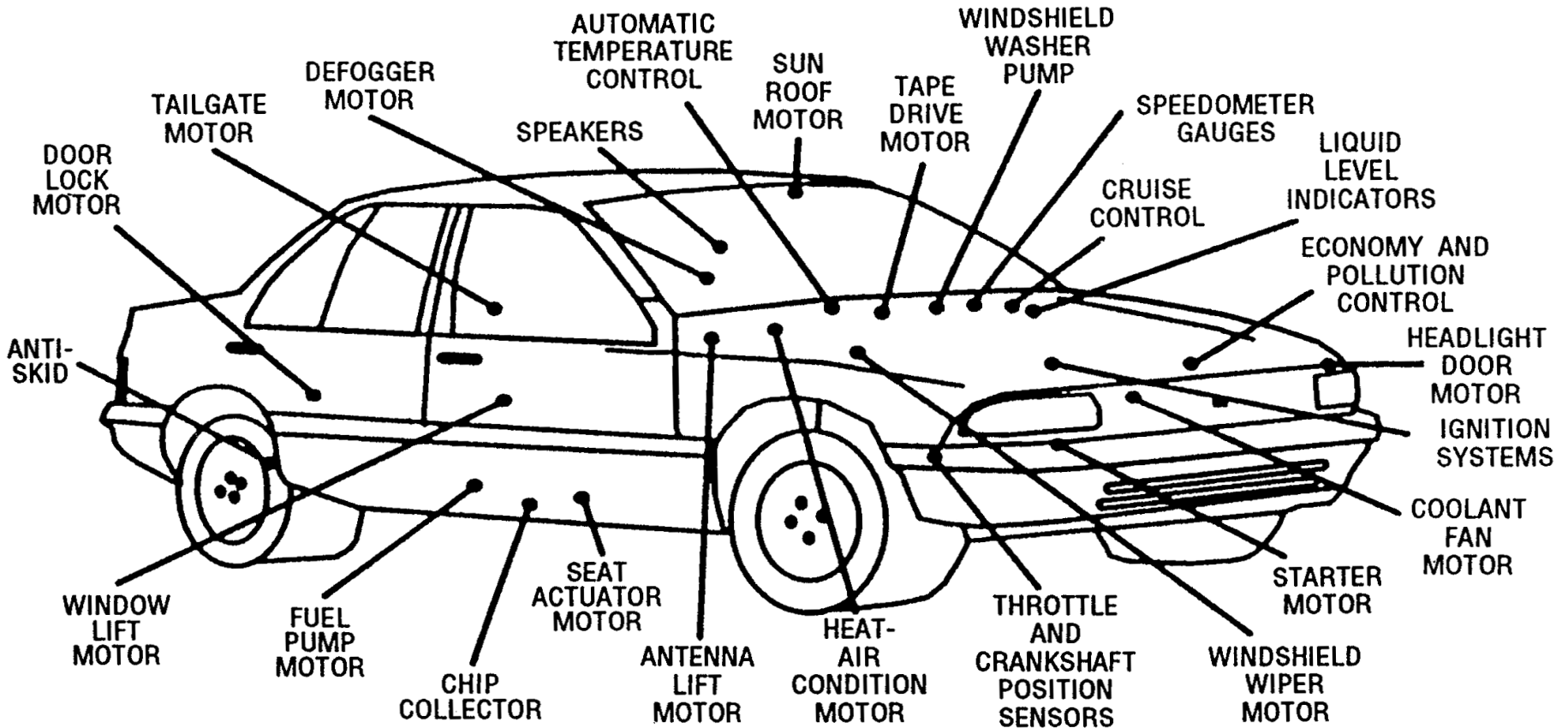
-reverse field to reduce magnetization to zero

Energy product BH_{MAX}

-(max. value of product (BH) in 2nd quadrant)

Bulk permanent magnets in motors

PERMANENT MAGNETS IN AUTOMOTIVE APPLICATIONS



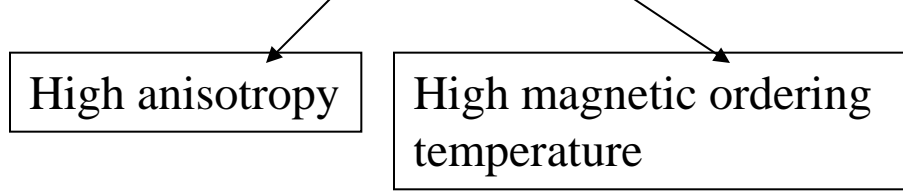
Why is nanostructuring important for bulk magnets?

Hard Magnetic Materials (permanent magnets)

Should have

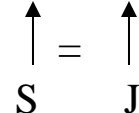
- a large coercivity (so they are not easily demagnetized)
- a large magnetization so that they create a strong magnetic field

Usually a combination of a rare-earth and a transition metal

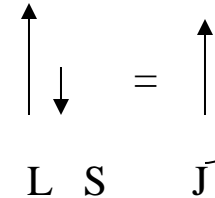


Magnetic structure

Transition metal



Light Rare-earth



Couple to give total moment

$\text{Nd}_2\text{Fe}_{14}\text{B}$ and SmCo_5 → important permanent magnet materials.
(tetragonal) (hexagonal)

Material	$\mu_0 M_s$ (T)	T_c (°C)	K_1 (MJ/m ³)	iH_c (MA/m)	$(BH)_{\max}$ (MG.Oe)
SmCo_5	1.0	700	10	2.9	24
$\text{Nd}_2\text{Fe}_{14}\text{B}$	1.6	312	5	1.6	45
CoPt	0.4	550	5	0.34	12

Nd₂Fe₁₄B-Structure

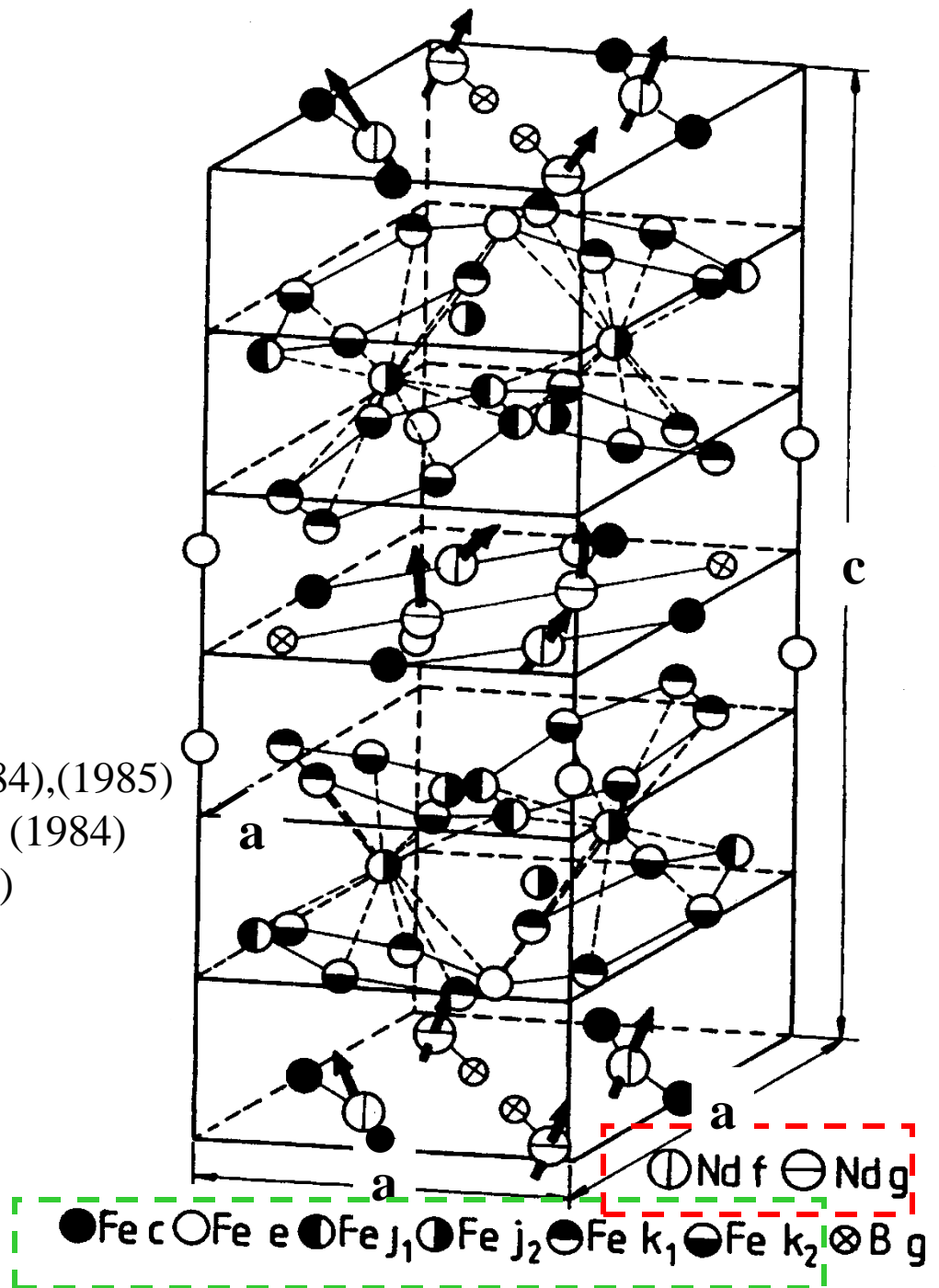
Tetragonal Structure.

See

Herbst et, Phys. Rev. B29,4176 (1984),(1985)

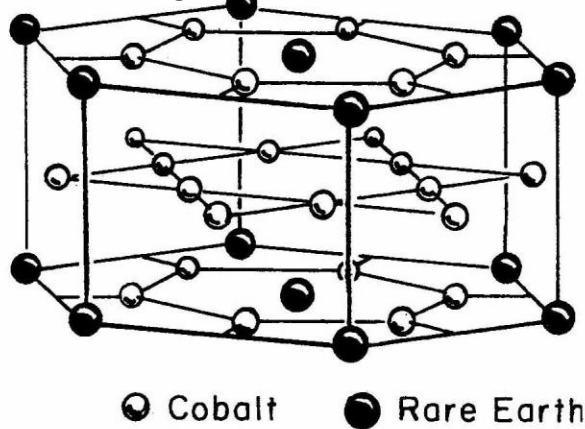
Shoemaker et, Acta Cryst C40,1665 (1984)

Givord et, Physica130B, 323, (1985)

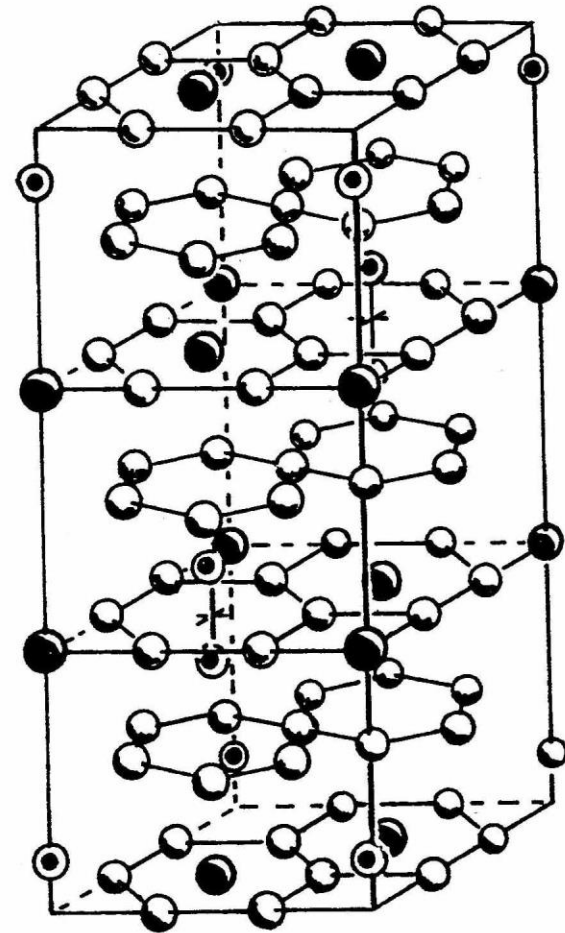


Structure of Sm-Co

SmCo_5 (hexagonal)



$\text{Sm}_2\text{Co}_{17}$ (rhombohedral)



See

O'Handley 'Modern Magnetic Materials', John Wiley and Sons (2000)

Barrett et al 'Structure of Materials', Pergamon Press (1980)

Strnat, 'Ferromagnetic Materials', Vol 4, Wohlfarth ed., Elsevier Press (1988)

Magnetic Recording

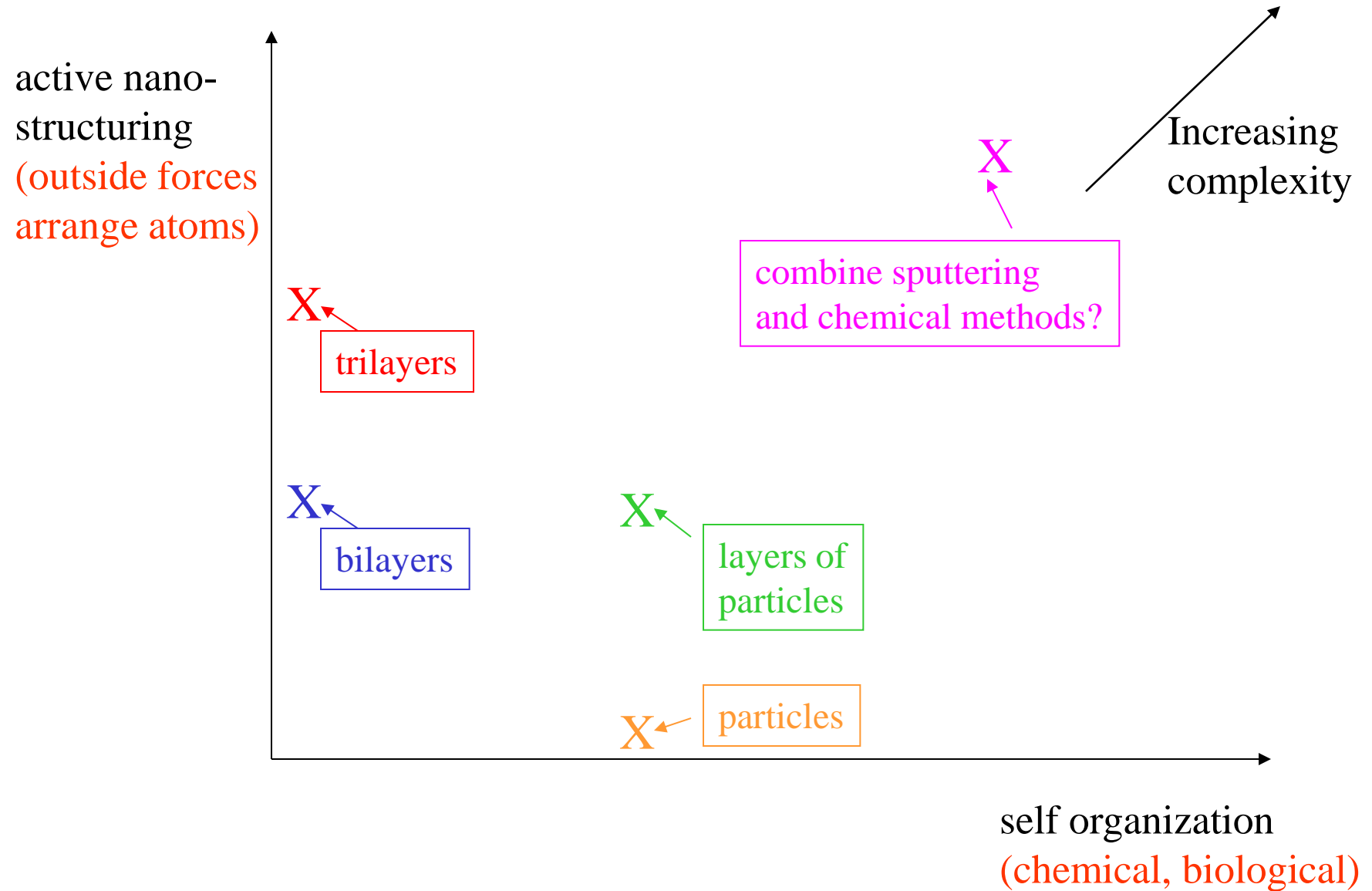
Recording medium- $\gamma\text{-Fe}_2\text{O}_3$ (maghematite), spinel structure
chemically stable
ferrimagnetic
anisotropy is from shape (10:1 ratio of dimensions)
coercivity 350 Oe
Cr added to increase the anisotropy

Type of recoding: longitudinal
perpendicular

Write head- e.g. miniature horseshoe magnet.
coil of wire energizes a high permeability magnet
(e.g. NiFe material)
field is created in the gap of the magnet
this field magnetizes the recoding medium
field created in gap $> H_c$ (recording medium)

Read head- i) write head could operate in reverse
ii) giant magnetoresistance read head

Preparation



2. Preparation and structure

This work

- Nb buffered,
- 540 nm thick NdFeB
- Influence of anneal time
- Increase Fe content

Standard (Vacuum)
anneal, 20 mins.

or
Rapid anneal, 30 seconds.

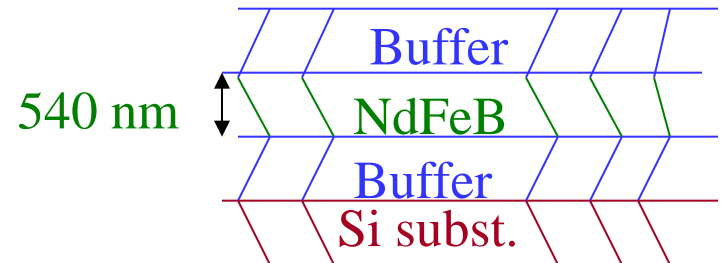
Four compositions:
Fe/Nd ratio: 6, 7.7, 9.4, 11.1 (PIXE)
Nd/B ratio: 1.8 (ICP mass spectroscopy)

Samples are of the form:

[Nb(20 nm)/NdFeB(d nm)/Nb(20 nm)]/Si subst

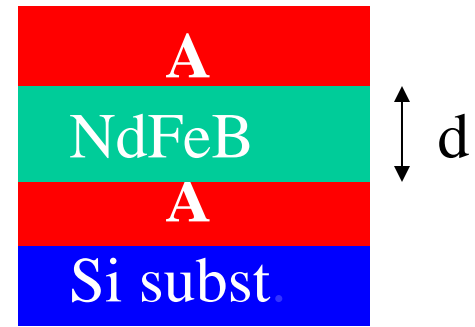
Preparation

- Ar ion sputtering
- Water cooled substrate
- Targets: NdFeB+Fe and Nb.



Preparation

Buffer layer provides protection



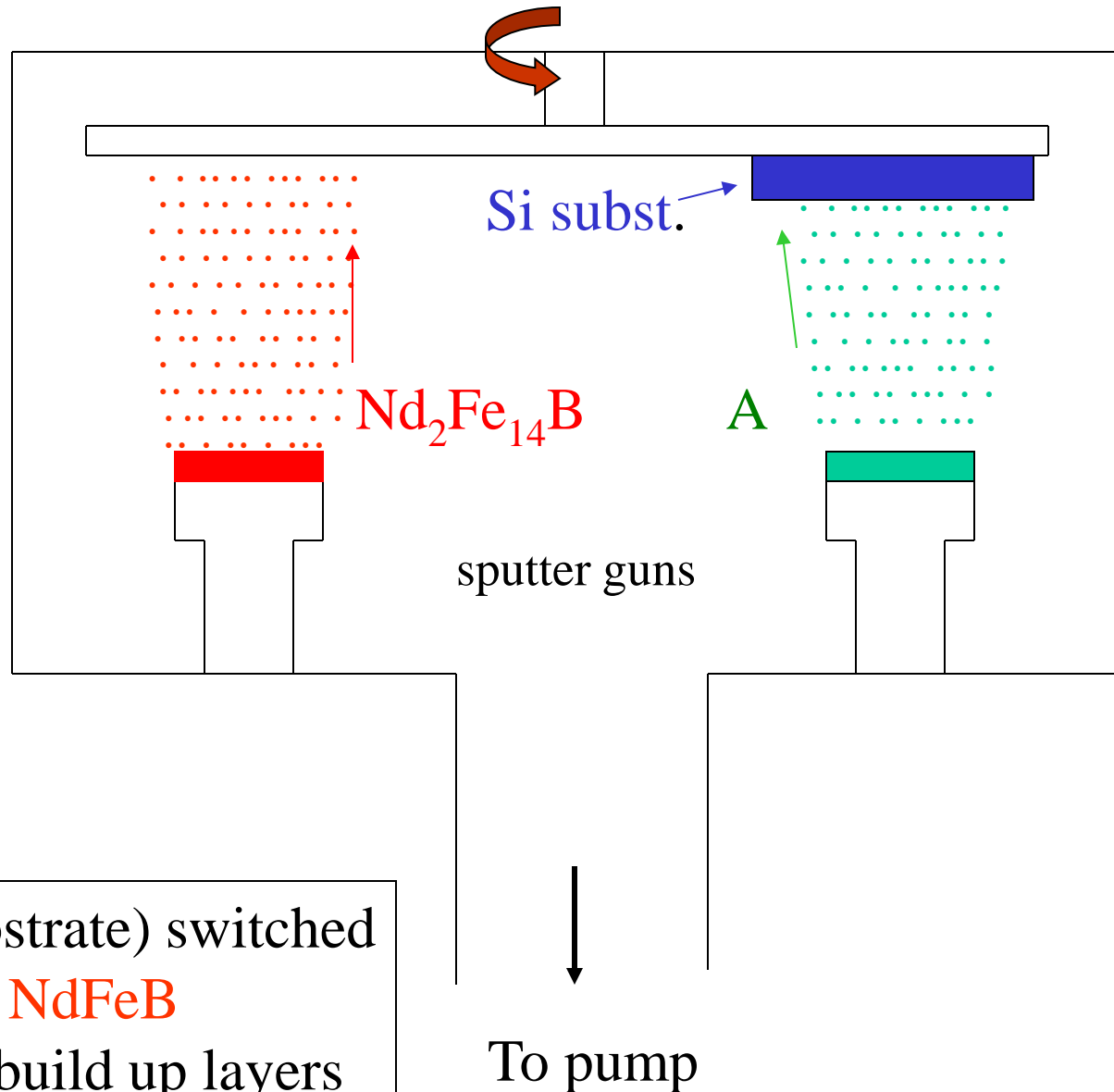
Change buffer layer A: Ti, V, Cr, Zr, Nb, Mo, Ta, Hf

Buffer layer materials:

- Nd has low solubility in them
- Mechanically hard, low reactivity

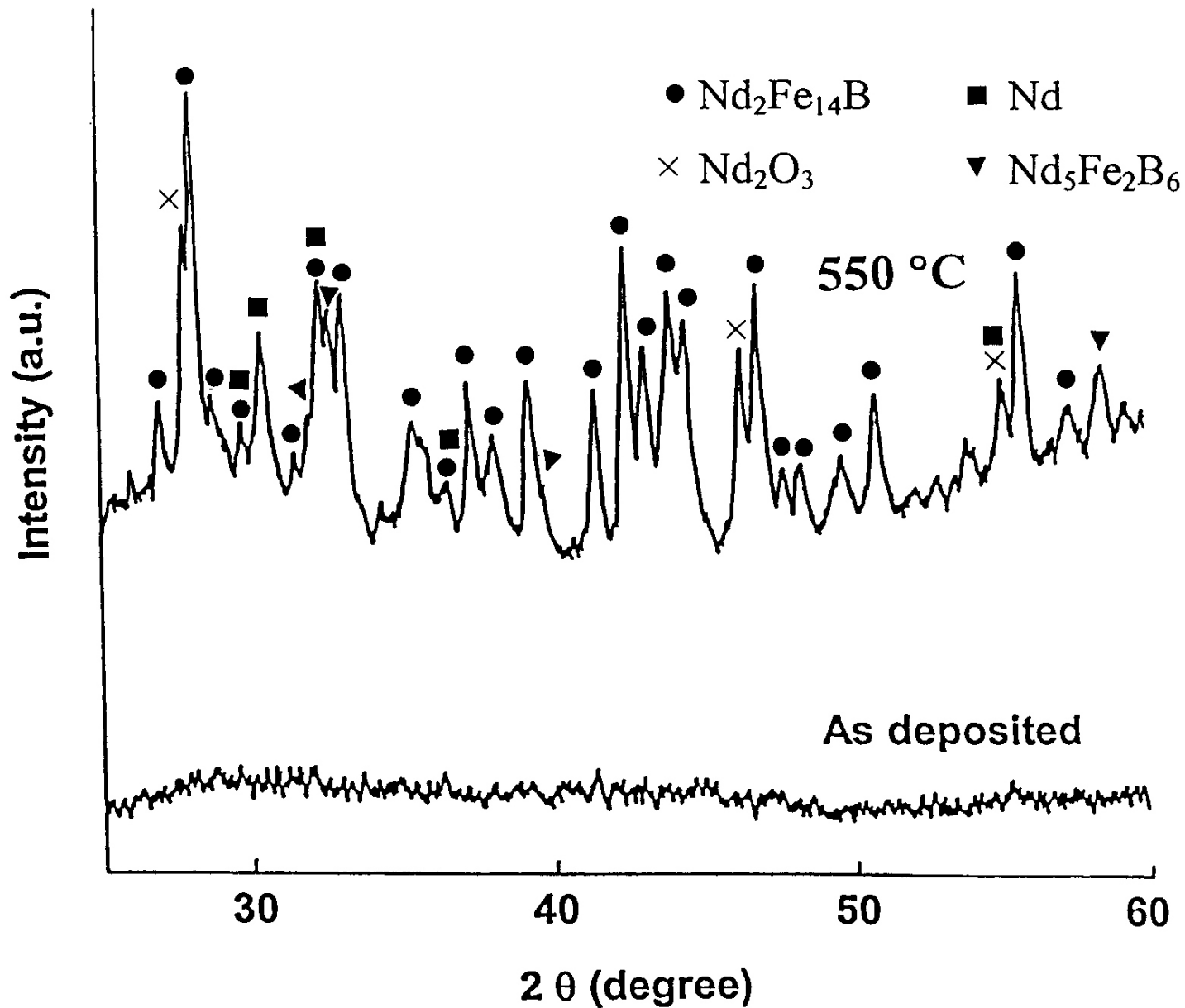
H ¹ 4K hcp 3.75 6.12																3.5/ 5.83						
Li 78K bcc 3.491	Be hcp 2.27 3.59																B rhomb. 4.05	C diamond 3.567	N 20K cubic 5.66 (N ₂)	O complex (O ₂)	F	Ne fcc 4.46
Na 5K bcc 4.225	Mg hcp 3.21 5.21																Al fcc 4.05	Si diamond 5.430	P complex	S complex	Cl complex (Cl ₂)	Ar 4K fcc 5.31
Crystal structure																						
← a lattice parameter, in Å →																						
← c lattice parameter, in Å →																						
K 5K bcc 5.225	Ca fcc 5.58	Sc hcp 3.31 5.27	Ti hcp 2.95 4.68	V bcc 3.03	Cr bcc 2.88	Mn cubic complex	Fe bcc 2.87	Co hcp 2.51 4.07	Ni fcc 3.52	Cu fcc 3.61	Zn hcp 2.66 4.95	Ga complex	Ge diamond 5.658	As rhomb.	Se hex. chains	Br complex (Br ₂)	Kr 4K fcc 5.64					
Rb 5K bcc 5.585	Sr fcc 6.08	Y hcp 3.65 5.73	Zr hcp 3.23 5.15	Nb bcc 3.30	Mo bcc 3.15	Tc hcp 2.74 4.40	Ru hcp 2.71 4.28	Rh fcc 3.80	Pd fcc 3.89	Ag fcc 4.09	Cd hcp 2.98 5.62	In tetr. 3.25 4.95	Sn (α) diamond 6.49	Sb rhomb.	Te hex. chains	I complex (I ₂)	Xe 4K fcc 6.13					
Cs 5K bcc 6.045	Ba bcc 5.02	La hex. 3.77 ABAC	Hf hcp 3.19 5.05	Ta bcc 3.30	W bcc 3.16	Re hcp 2.76 4.46	Os hcp 2.74 4.32	Ir fcc 3.84	Pt fcc 3.92	Au fcc 4.08	Hg rhomb.	Tl hcp 3.46 5.52	Pb fcc 4.95	Bi rhomb.	Po sc 3.34	At —	Rn —					
Fr	Ra	Ac																				

Sputter Deposition

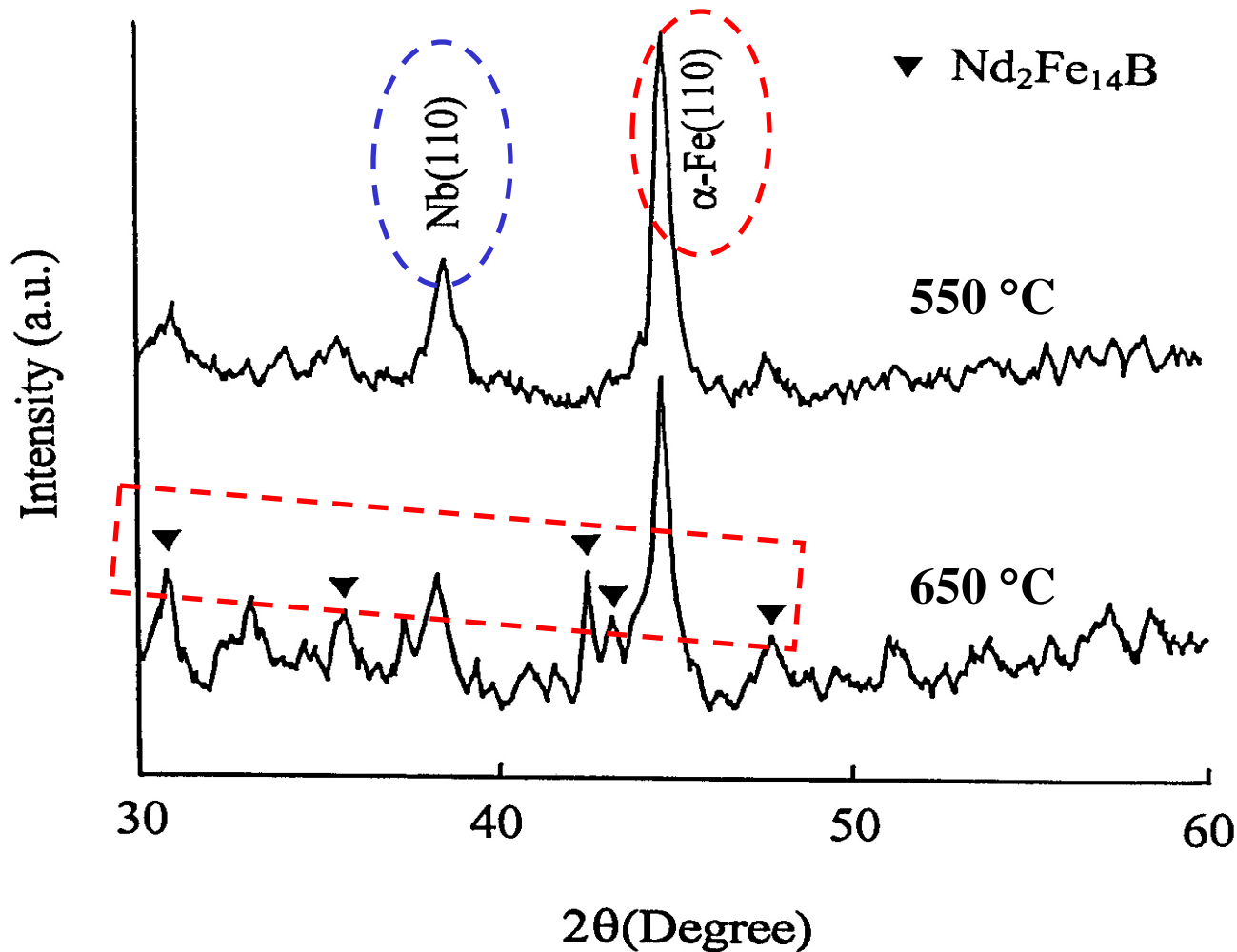
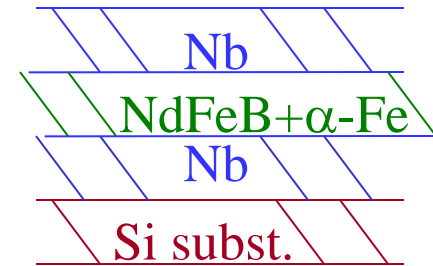


Sample (Si substrate) switched between **A** and **NdFeB** sputter guns – build up layers in this way

X-ray diffractogram Mo(20nm)/NdFeB(180nm)/Mo(20nm)
-crystallite size 30 nm



Cu K_{α} x-ray diffraction
 $Nd_2Fe_{19}B$ (20 min. anneal).



Samples with extra Fe have both $Nd_2Fe_{14}B$ and α -Fe phases

3. Annealing rate and varying non-magnetic layer

Parameters varied and their physical effect

Parameter	Range	Possible effect
A (buffer)	Cr,Mo,Nb,Ta,Ti, V,Zr,SiC,BN	Morphology, Buffer/NdFeB mix
d (thickness)	54, 90, 180, 540nm	Magnetic size effect, morphology
T _{an} (anneal)	450 to 750°C	Morphology
Anneal time	20 mins or 30 secs	Morphology
Fe content	Four compositions	α -Fe formation, BH _{max} enhance.

Annealing

Vacuum anneal(20 minutes)

or

Rapid thermal anneal (30 seconds)

Purpose

Crystallize the tetragonal $\text{Nd}_2\text{Fe}_{14}\text{B}$

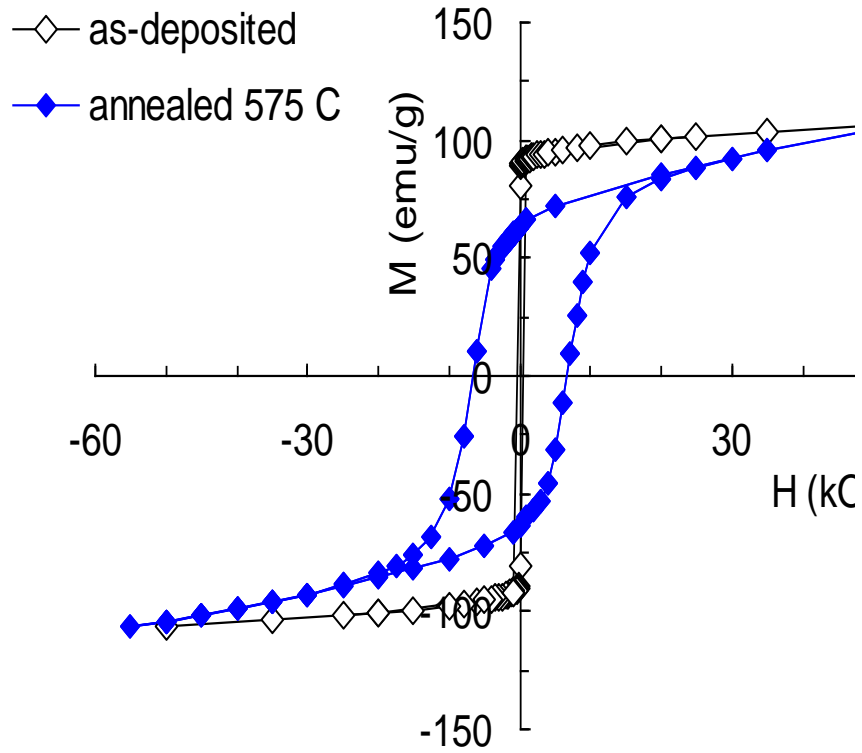
Improve crystal quality (remove defects) from $\text{Nd}_2\text{Fe}_{14}\text{B}$

Problem related to annealing:

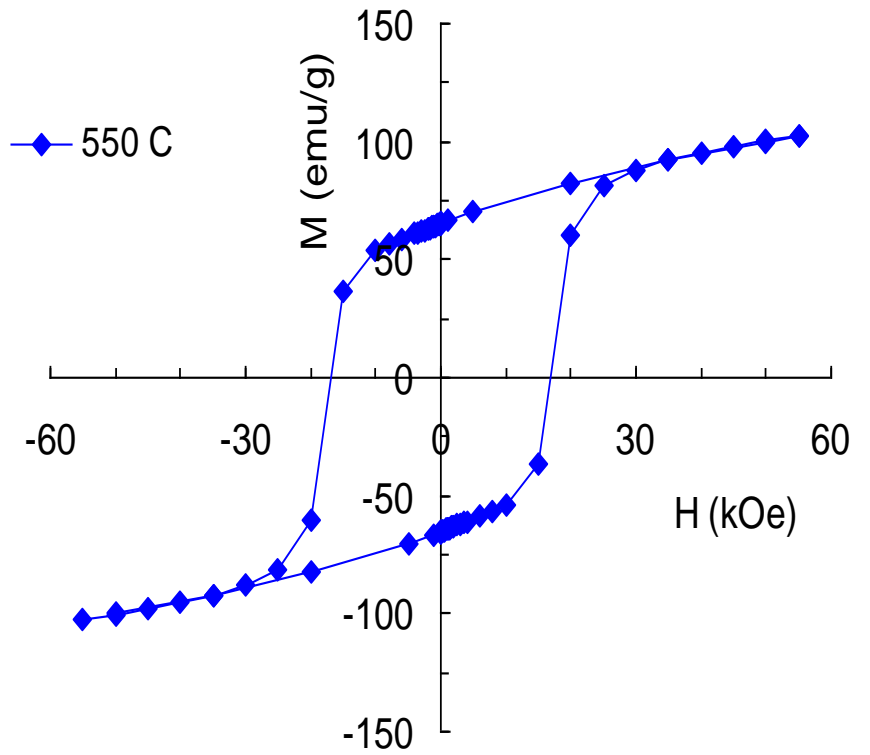
can lead to a mixing of the buffer layer and the magnetic ($\text{Nd}_2\text{Fe}_{14}\text{B}$) phase.

Can lead to sample-substrate adhesion problems

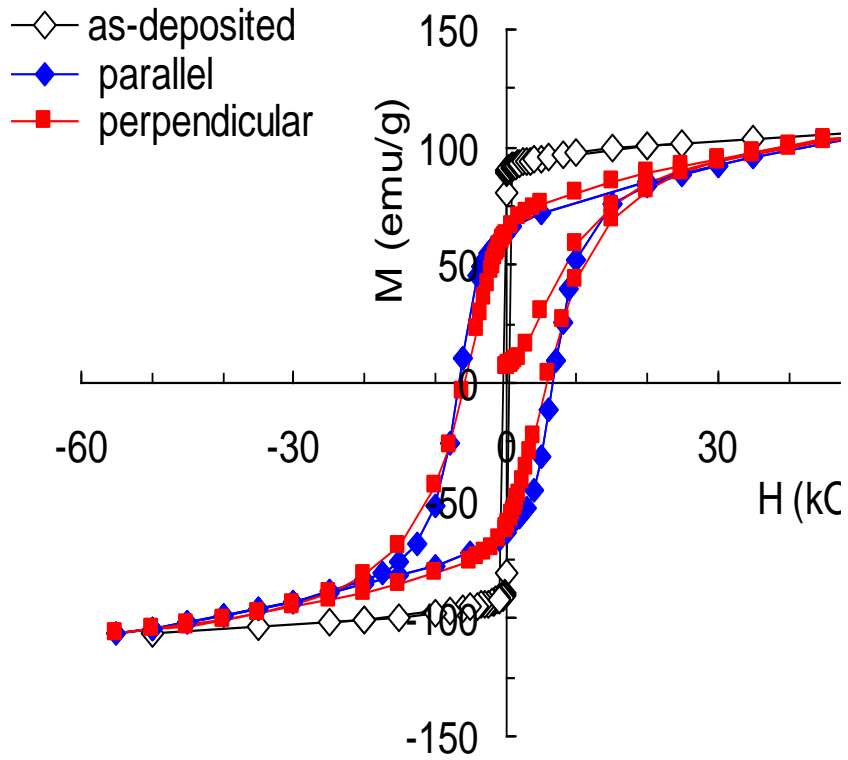
Cr/NdFeB(180 nm)/Cr



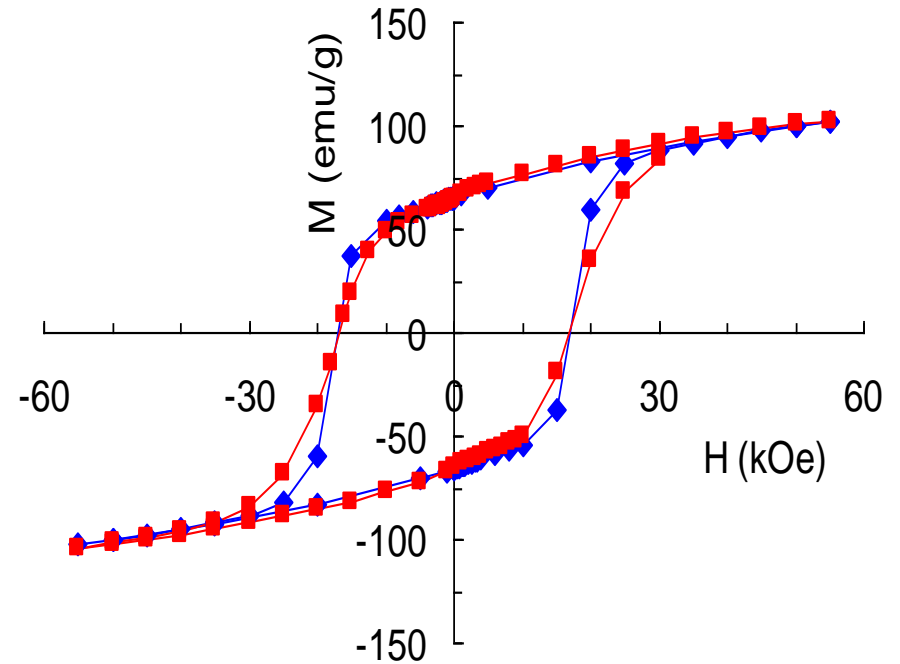
Mo/NdFeB(180 nm)/Mo



Cr, 180 nm, annealed 575 C



Mo, 180 nm, annealed 550 C



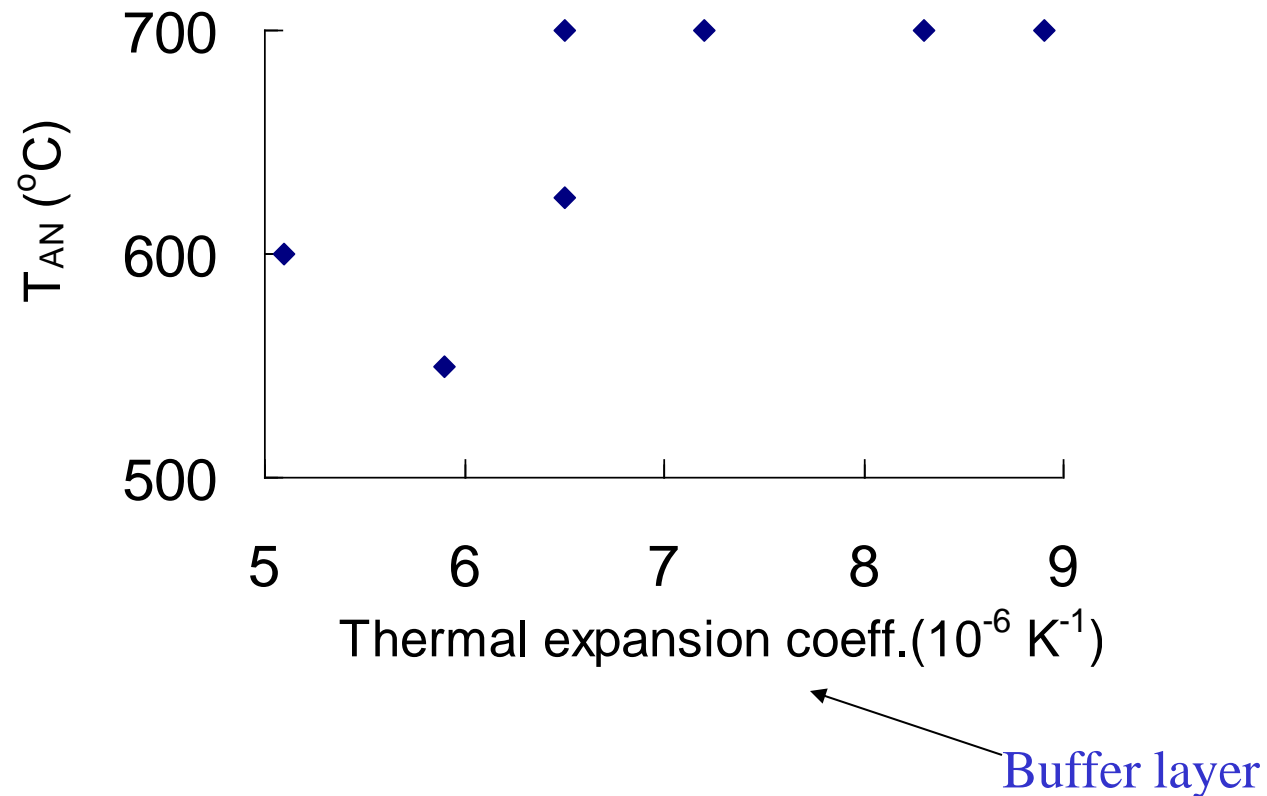
Coercivity summary

Buffer, H_{Ci}

Ti 15 kOe	V 2 kOe	Cr 6.7 kOe
Zr - -	Nb 20 kOe	Mo 17 kOe
Hf 14 kOe	Ta 10 kOe	W* 7.4 kOe *Tsai et al, Jour. Magn.Mag.Mater 196, 728 (1999).

Anneal temperature and Adhesion

Anneal temp at which sample no longer adheres to the substrate



Theoretical Prediction of BH_{\max}

-Largest value of BH in second quadrant

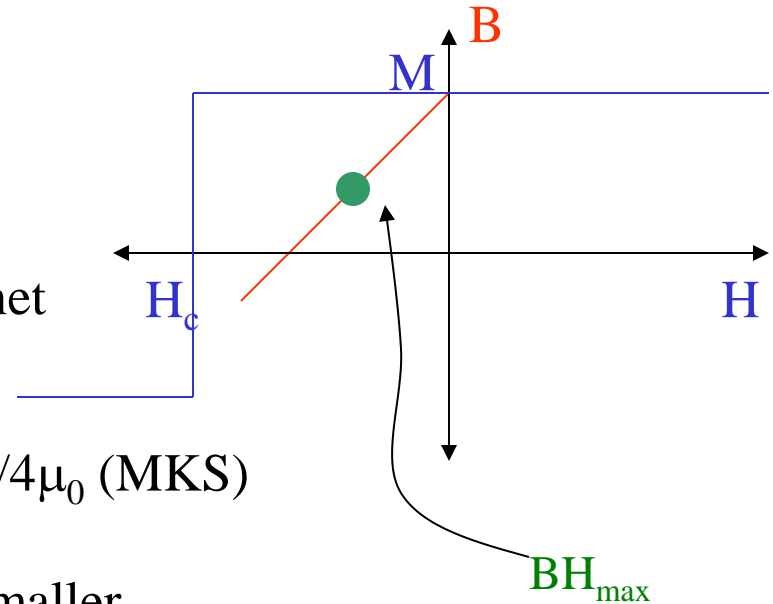
-measures magnetostatic energy stored in magnet

-If coercivity is sufficiently large, $BH_{\max} = M_s^2/4\mu_0$ (MKS)

-If coercivity is less than $M_s/2$, then BH_{\max} is smaller

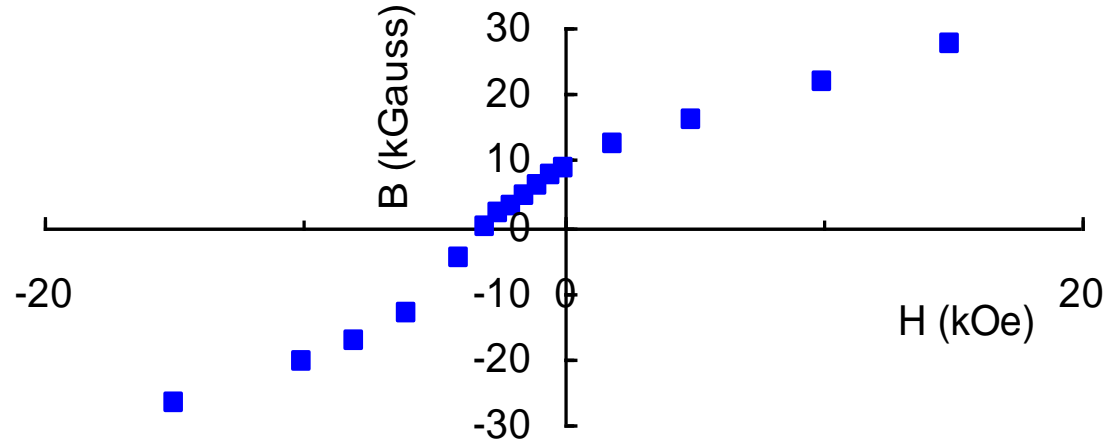
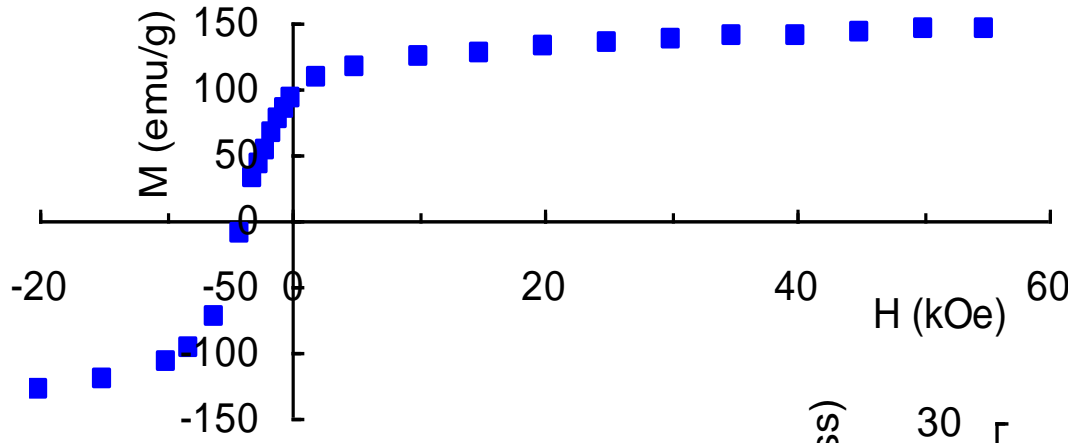
e.g. if Fe had a large enough coercivity, $BH_{\max} = 0.92 \text{ MJ/m}^3$,
measured value is $\sim 0.001 \text{ MJ/m}^3$
[Skomski, Coey, Phys. Rev. B 48, 15812 (1993)]

e.g. bulk $\text{Nd}_2\text{Fe}_{14}\text{B}$: BH_{\max} (upper limit) = 0.516 MJ/m^3
measured value 0.405 MJ/m^3
[Sagawa et al, Japan. J. Appl. Phys. 26, 785 (1987)]

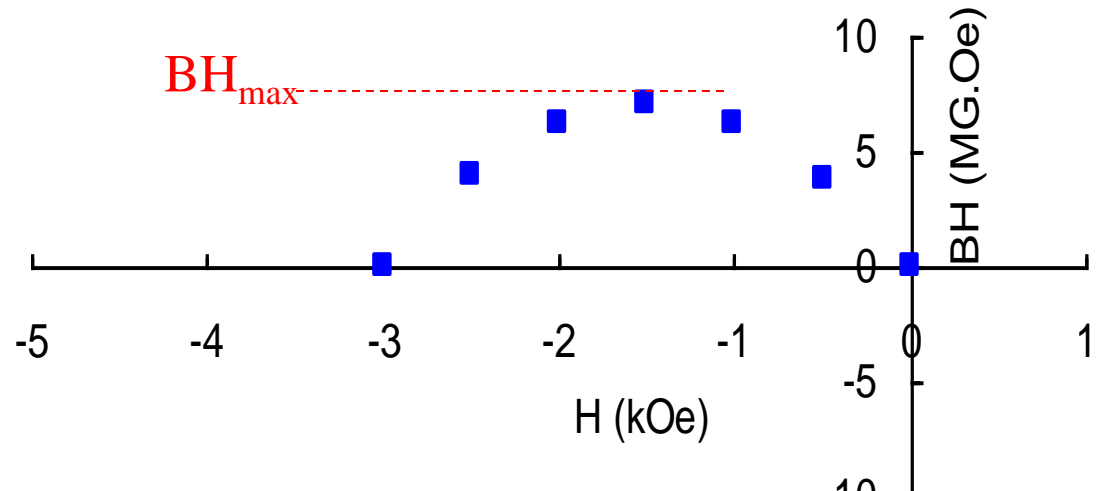


Maximum Energy Product, BH_{max}

Nb/NdFeB(540 nm)/Nb
625 C, 20 mins



$$1 \text{ MG.Oe} = 7.96 \text{ kJ/m}^3$$



Best Values of H_c , BH_{max} for each buffer

Buffer, H_{Ci} , Max (BH_{MAX})

Ti 15 kOe 9.3 MG-Oe	V 2 kOe 2.1 MG-Oe	Cr 6.7 kOe 6.8 MG-Oe
Zr - -	Nb 20 kOe 7.7 MG-Oe	Mo 17 kOe 10.3 MG-Oe
Hf 14 kOe 6.8 MG-Oe	Ta 10 kOe 3.2 MG-Oe	W* 7.4 kOe *Tsai et al, Jour. Magn.Mag.Mater 196, 728 (1999).

[Jiang, O'Shea, J. Magn. Magn. Mater. 59, 212, (2000)]

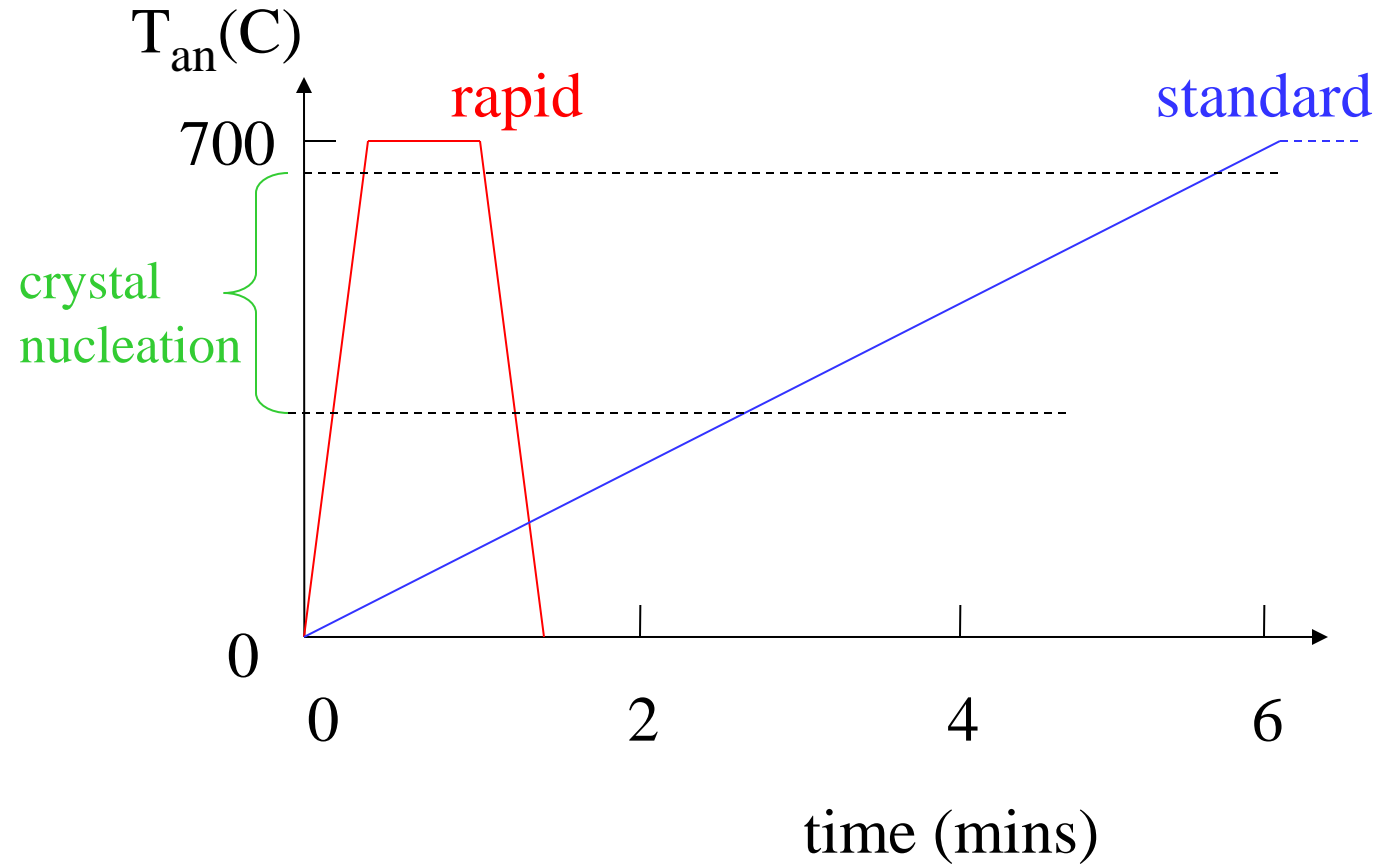
Annealing

Vacuum anneal(20 minutes)

or

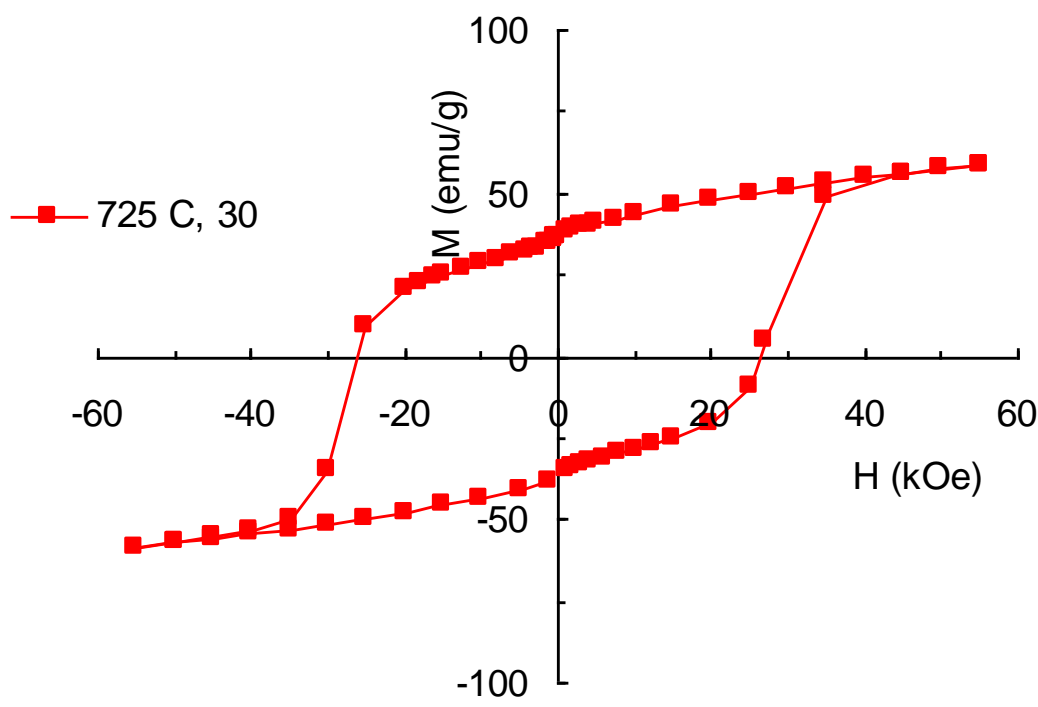
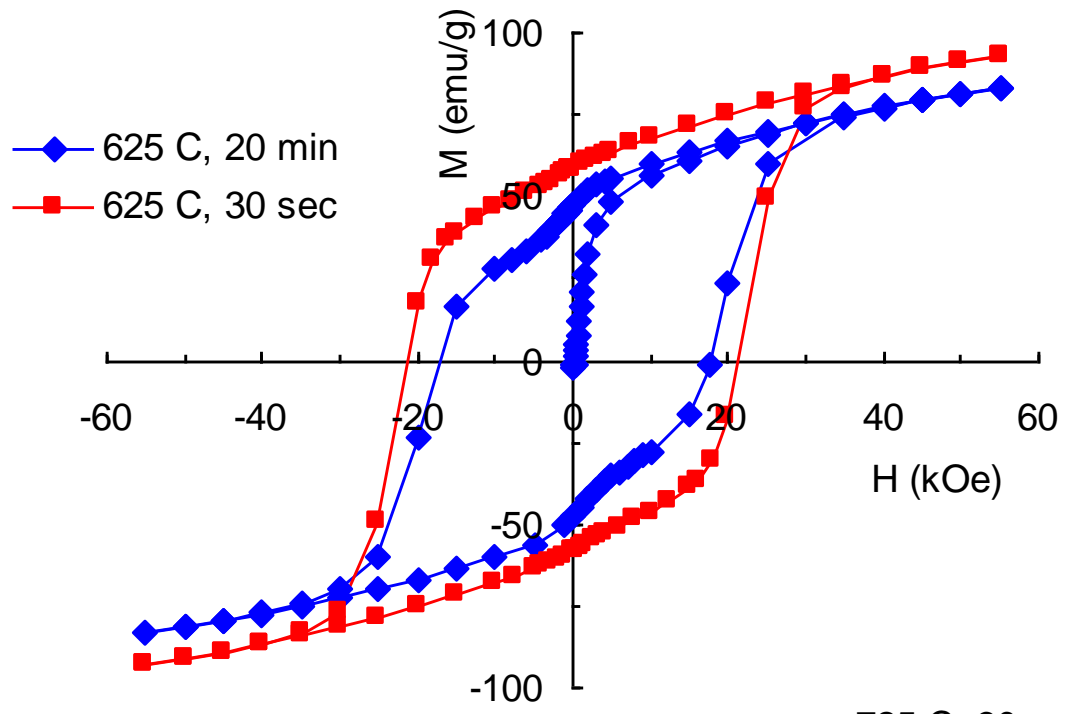
Rapid thermal anneal (30 seconds)

Anneal Temperature profiles

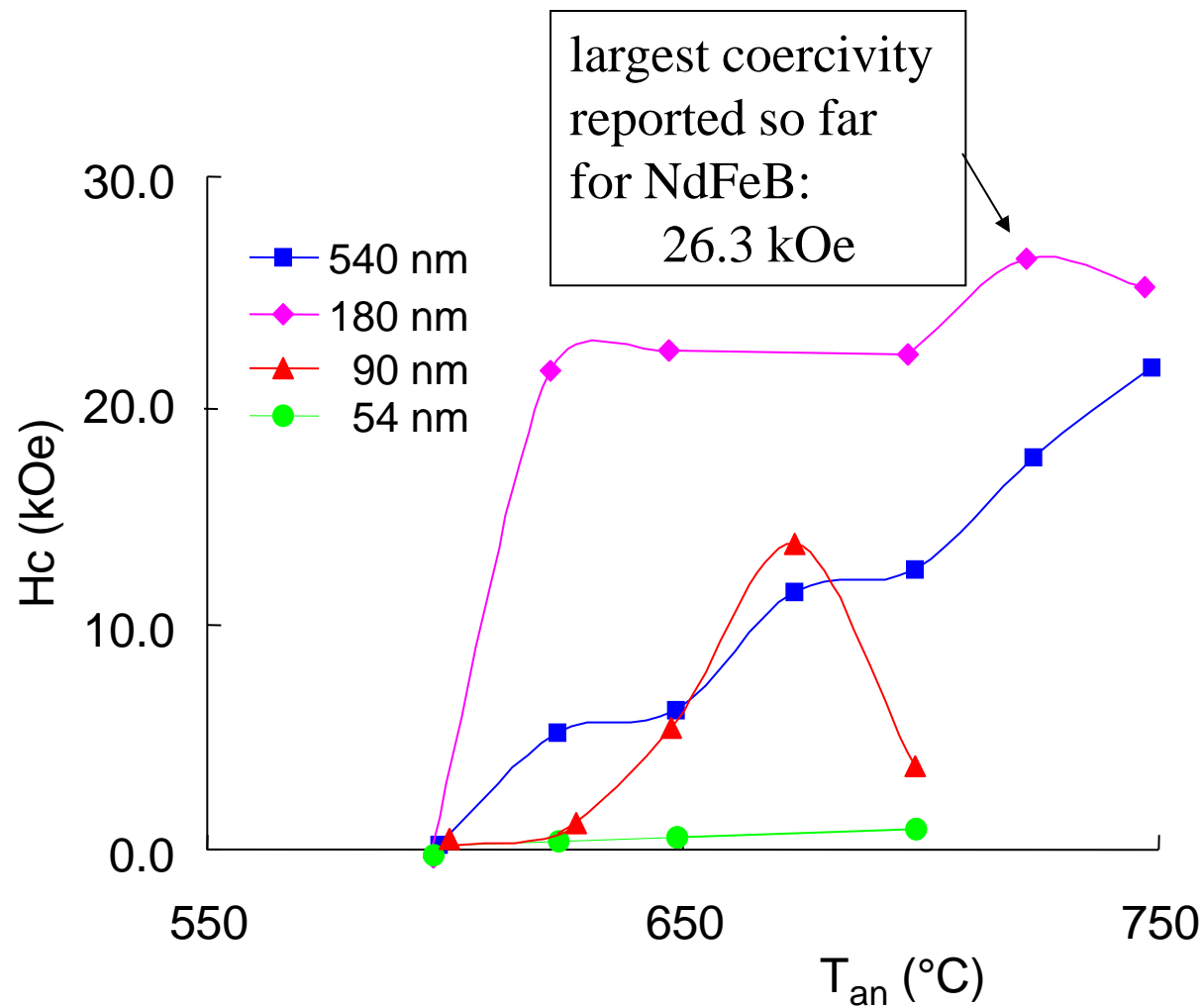
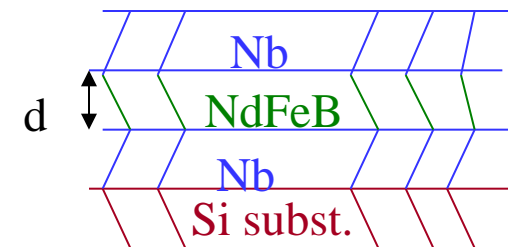


- a rapid anneal should lead to more uniform grain size.

Rapid anneal



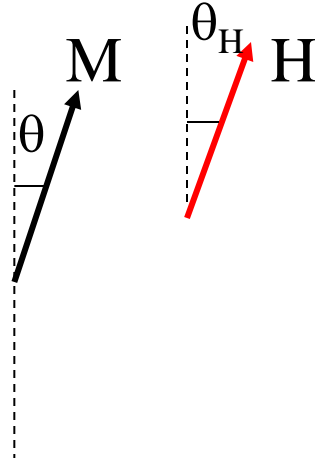
H_C as a function of T_{an} , (rapid anneal)



To find coercivity for a simple model

Single magnetic domain:

$$E_a = K \sin^2\theta$$
$$E_h = -MH \cos\theta_H$$

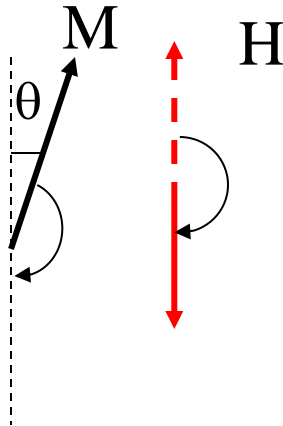


Magnetic domains randomly oriented.

$$H_C = H_{C1}/2 = (K_1 + K_2)/M$$

Reverse H :

$$H = 2K/M$$
$$H_{C1}$$



For $\text{Nd}_2\text{Fe}_{14}\text{B}$ (theory):

$$H_C = 32.4 \text{ kOe}$$

Maximum coercivity

Theoretical maximum (randomly oriented grains) 32.4 kOe

Experiment 26.3 kOe (our thin film), $\text{Nd}_2\text{Fe}_{8.3}\text{B}_{0.8}$

[Jiang, Evans, O'Shea, Du, J. Magn. Magn. Mater. 224, 233 (2001)]

Other work: 27.5 kOe (bulk melt-spun), $\text{Nd}_{147}\text{Fe}_{13}\text{B}$

[Girt, Krishnan, Thomas, Altounian, Appl. Phys. Lett. 76, 1737 (2000)]

3. Modeling the coercivity

Magnetic Reversal by Uniform Rotation

[(W. F. Brown, Rev. Mod. Phys. 17, 15 (1945)]

Assuming a single particle with field applied along the uniaxial axis:

$$H_C = 2K_1/M_S - N_e M_S$$

K_1 - uniaxial anisotropy coefficient

M_S - saturation magnetization

N_e - difference between parallel and perpendicular demagnetization factors

Modified Brown's Equation

(H. Kronmuller, K.-D. Durst, J. Magn. Magn. Mater. 74, 291 (1988))

$$H_C = (2K_1/M_S)\alpha_\psi\alpha_K - N_e M_S$$

α_ψ - grains not aligned (randomly oriented, $\alpha_\psi \sim 0.5$)

α_K - grains are not perfect

Both α_ψ and α_K reduce coercivity

Pinning: $\alpha_K < 0.3$

Nucleation: no restriction on α_K

Magnetic reversal by nucleation

[(D. Givord, P. Tenaud, T. Viadieu, IEEE Trans. Mag. 24, 1921 (1988))]

Here reverse magnetic domains
nucleate and expand.

$$H_C = \gamma_B \alpha_S \alpha_B / \mu_0 v^{1/3} M_S - N_{\text{eff}} M_S$$

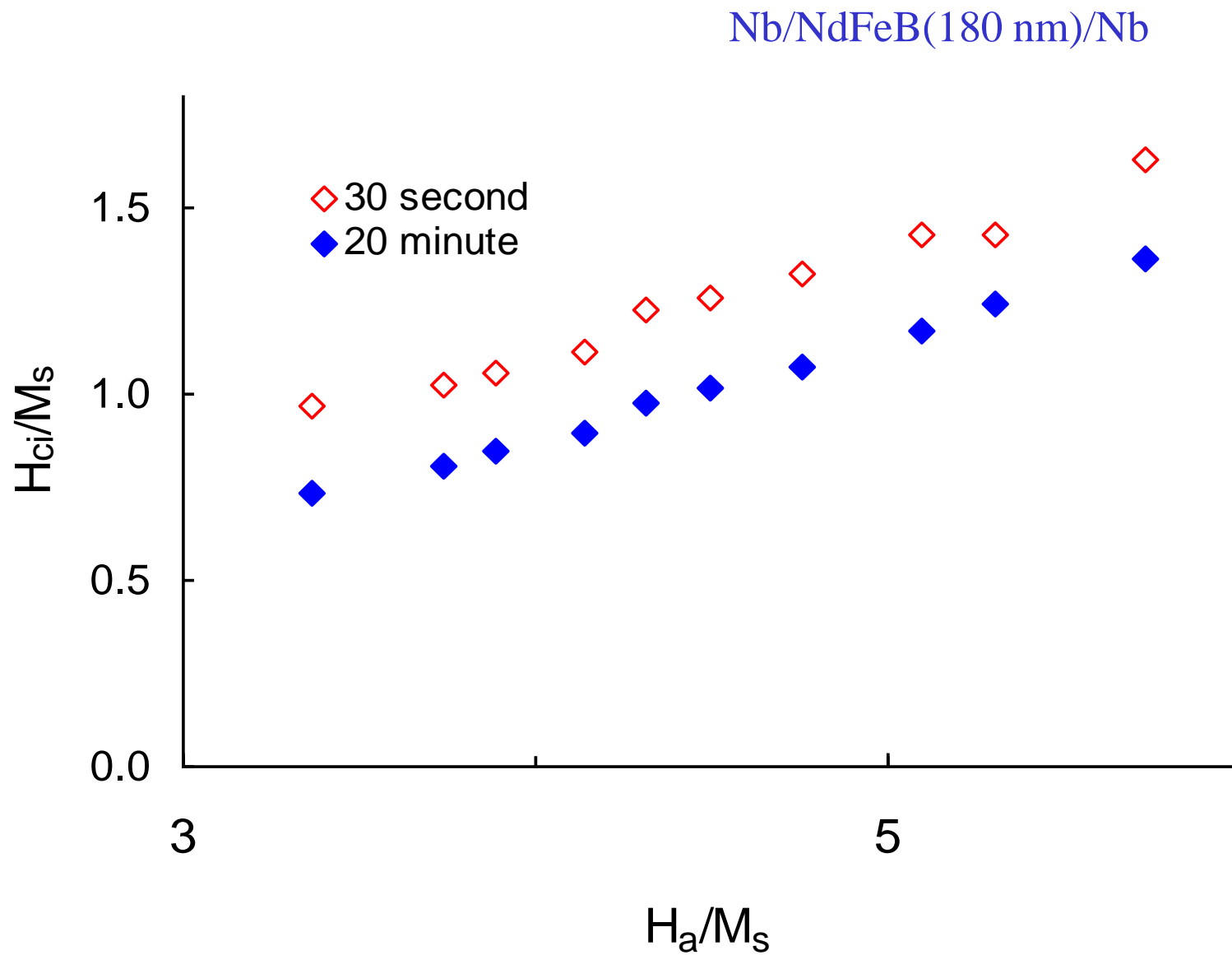
γ_B – domain wall energy of ideal material

α_S – geometric factor ($= s/v^{2/3}$, s is
nucleus surface area and v is volume)

α_B – relates wall energy to ideal wall energy

Both are similar in form!

Modified Brown' plot



Modified Brown's Plot

Assume $\alpha_\psi = 0.5$ (no texture)

d (nm)	Anneal Time (min)	Anneal temp (°C)	H_{ci} (kOe)	M_h (emu/g)	M_r/M_h	N_e	α_K α_{ex}
180	20	600	18.0	91.5	0.58	0.19	0.54
180	0.5	650	21.4	100.7	0.63	0.07	0.59

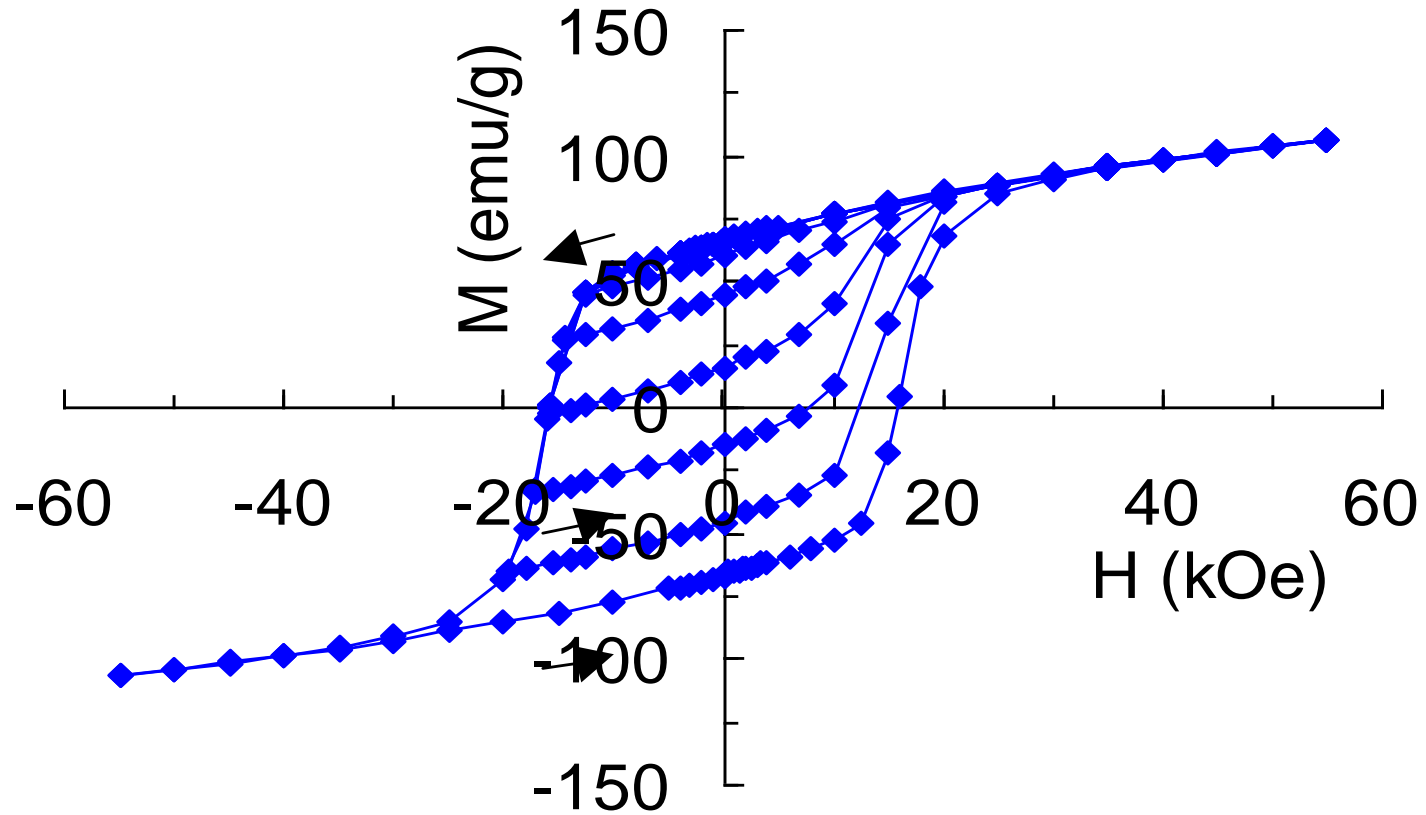
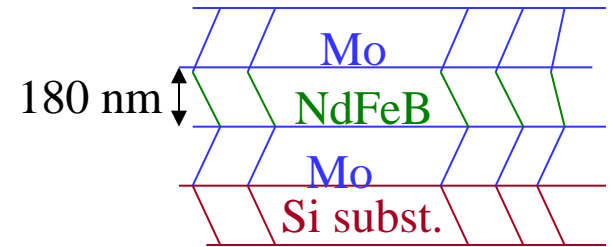
The rapidly annealed sample has:

smaller N_e indicating smaller internal demagnetization fields

larger α_K (indirect argument) suggesting that the grains are of higher quality.

larger remanence ratio

Annealed 550 C



Largest 'Maximum Energy Product', BH_{MAX} :

13 MGauss-Oe (103 kJ/m^3)

Buffer: Nb

Anneal time,temp:30 sec, 750 °C

Composition: $\text{Nd}_2\text{Fe}_{18}\text{B}_{0.8}$ (Fe-rich)

Grain size 35-50 nm, randomly oriented.

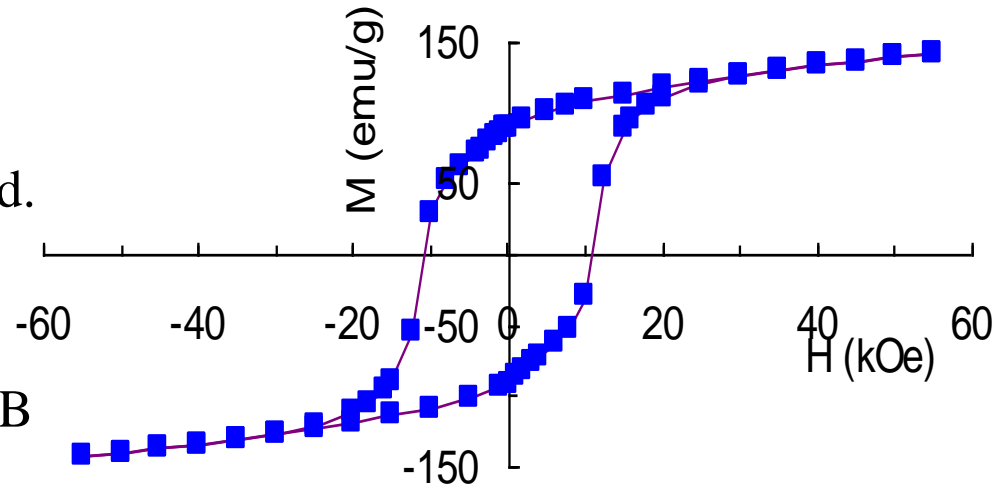
α -Fe is present

- Exchange between α -Fe and $\text{Nd}_2\text{Fe}_{14}\text{B}$ phases leads to a large BH_{MAX} ,

- Coercivity is 11 kOe

- Others have reported 22.8 MGauss-Oe in oriented films with coercivity of 9.4 kOe.

- Next: Orient the grains to increase BH_{MAX}



4. Exchange coupling

Combine crystallites of $\text{Nd}_2\text{Fe}_{14}\text{B}$ and Fe

Large anisotropy
and coercivity

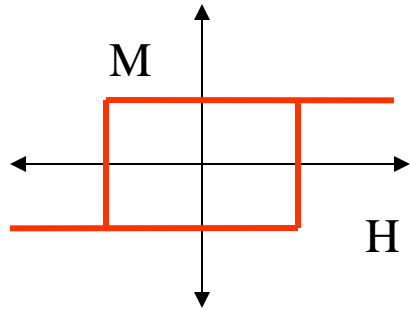
Large magnetic
moment

Composite material has a large interface area,
two phases should be strongly coupled magnetically,

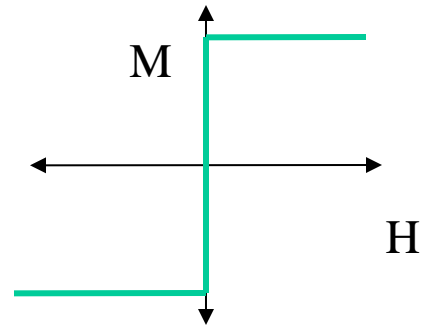
Result: a material with large coercivity, and moderately large magnetization
[Kneller, Hawig, IEEE Trans. Magn. 27, 3588 (1991)]

Two separate materials:

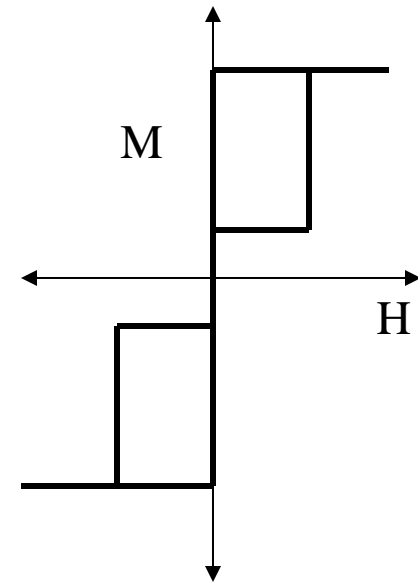
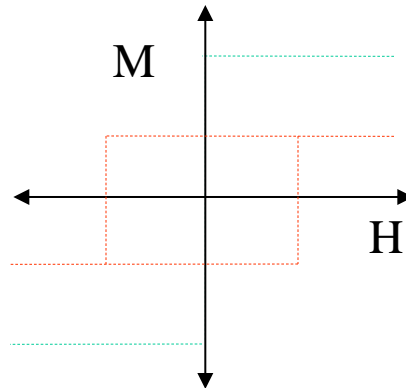
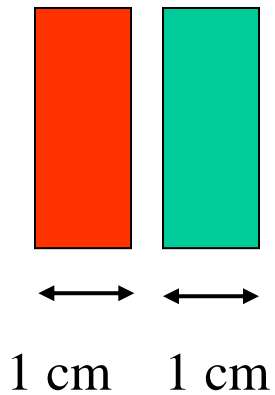
hard (e.g. $\text{Nd}_2\text{Fe}_{14}\text{B}$)



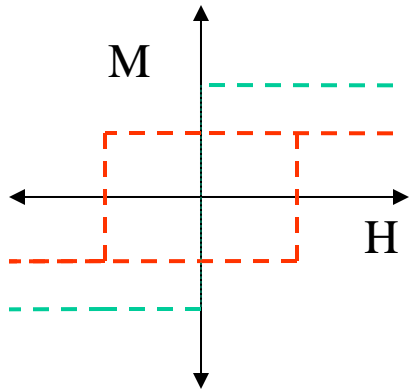
soft (e.g. Fe)



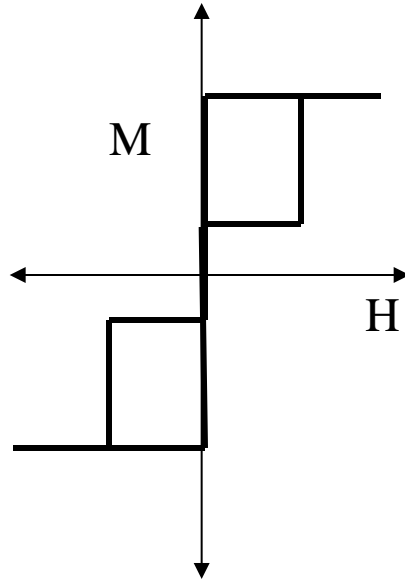
Put them together:



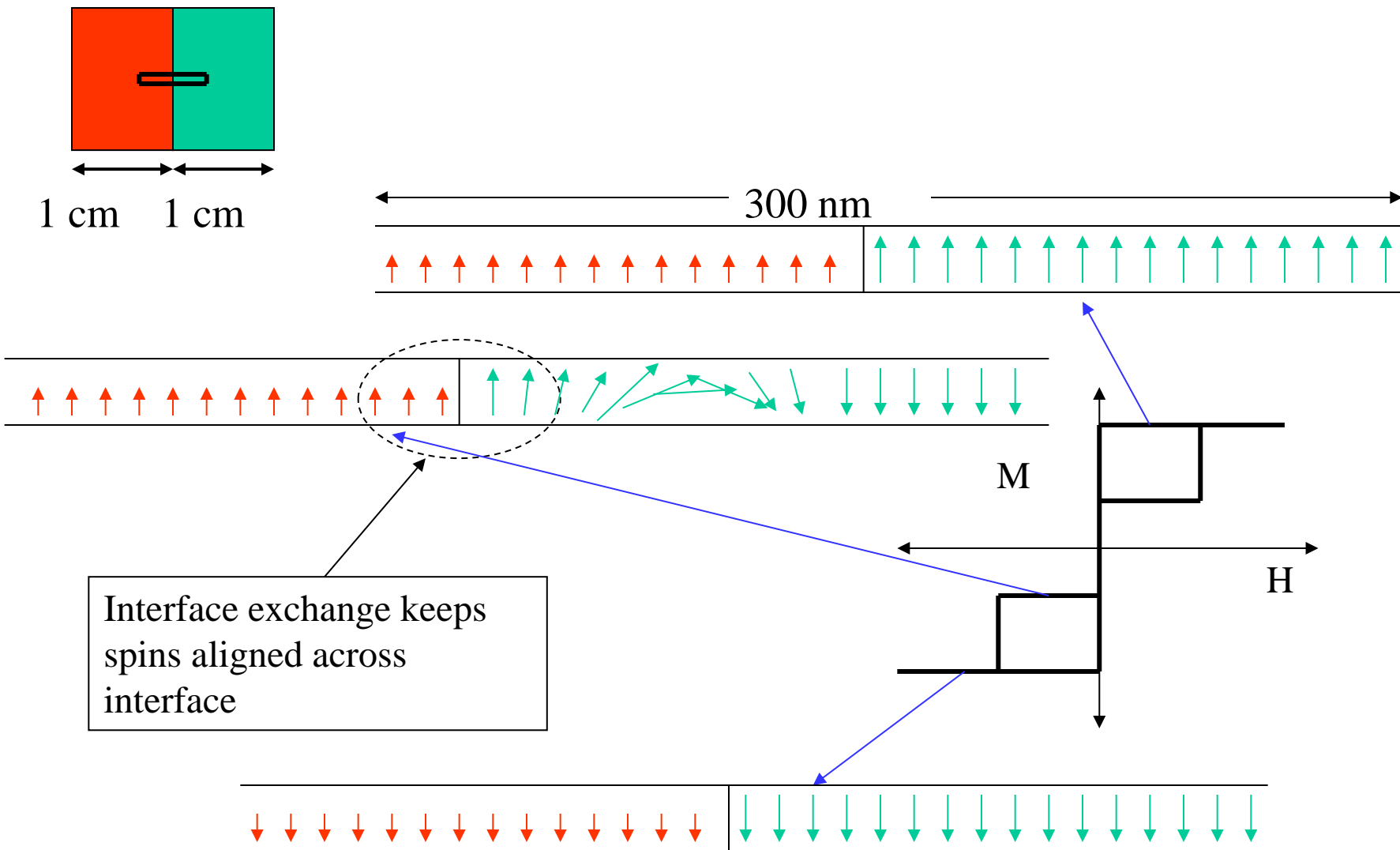
separate loops



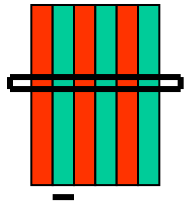
added together



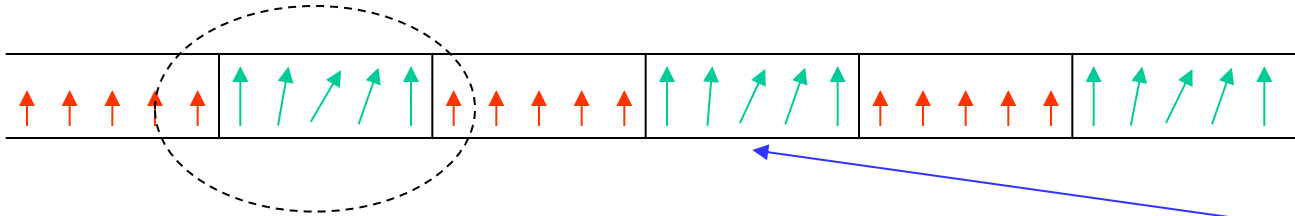
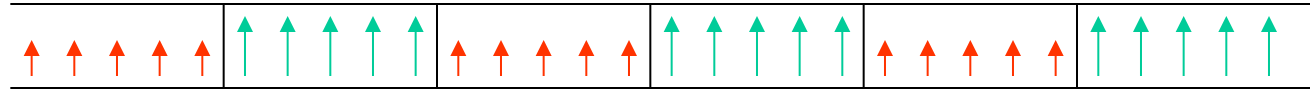
Microscopic view of interface:



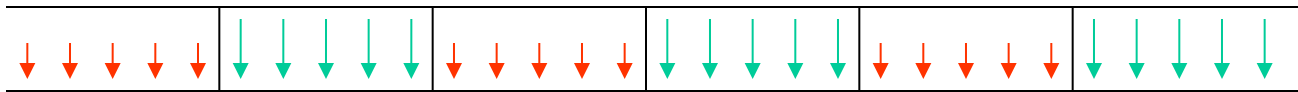
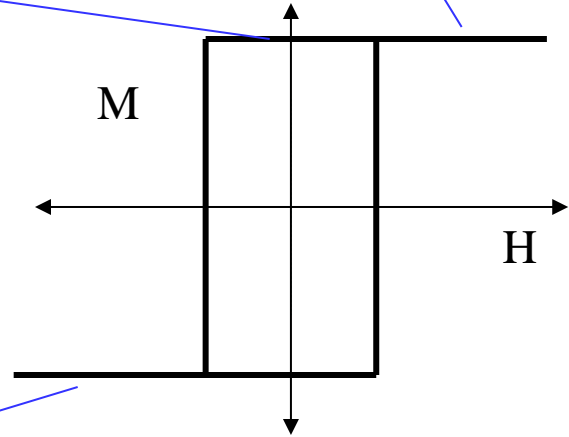
Now lets make the layers 30 nm thick:



30 nm

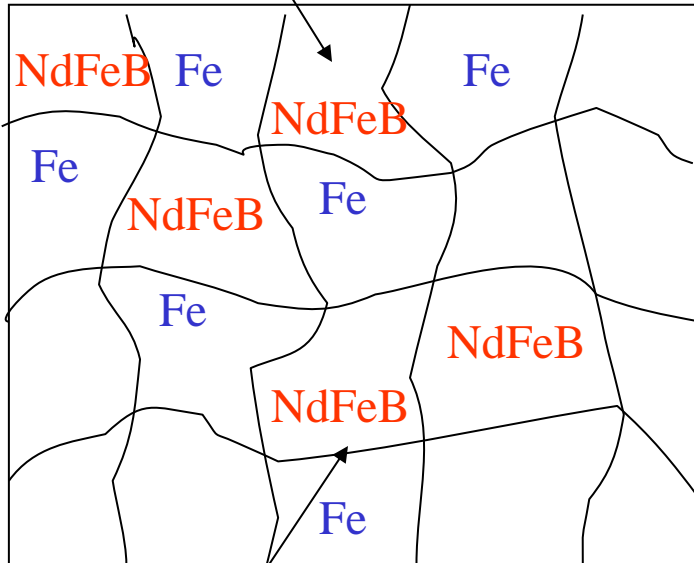


Small amount of canting across width of soft layer

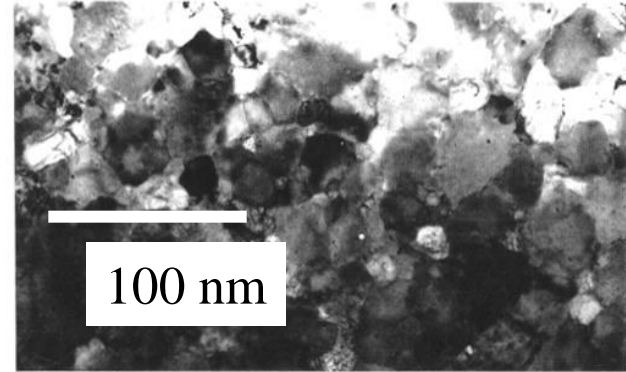


Permanent Magnet

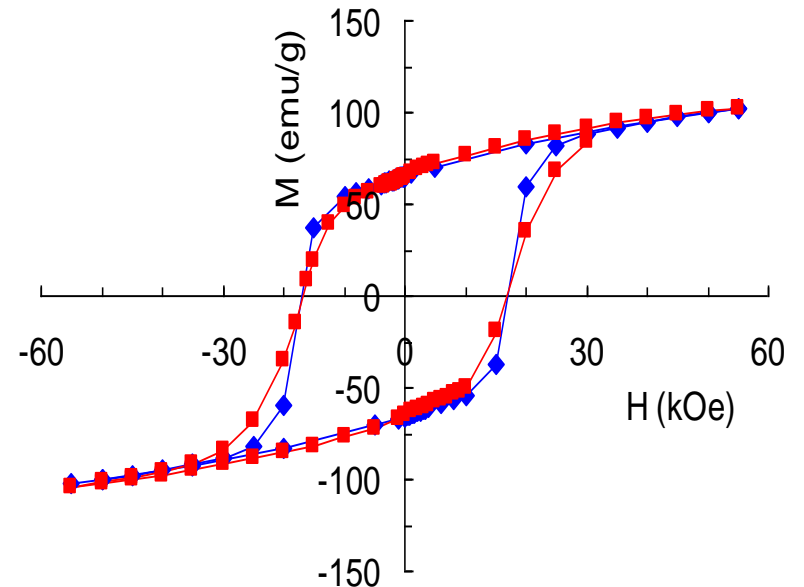
Small crystallite size
→ high coercivity



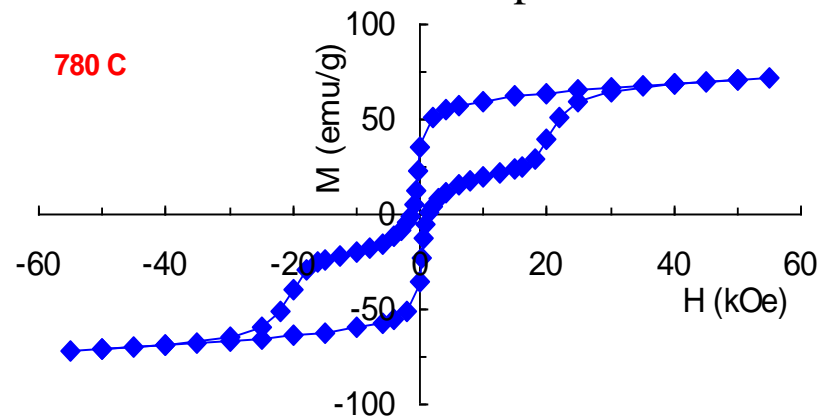
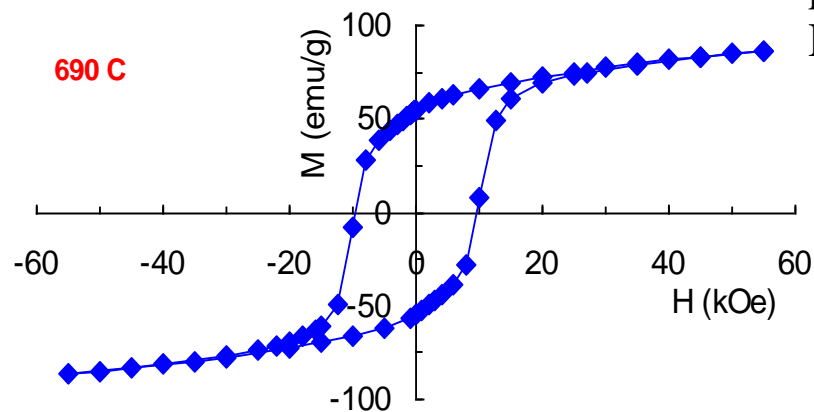
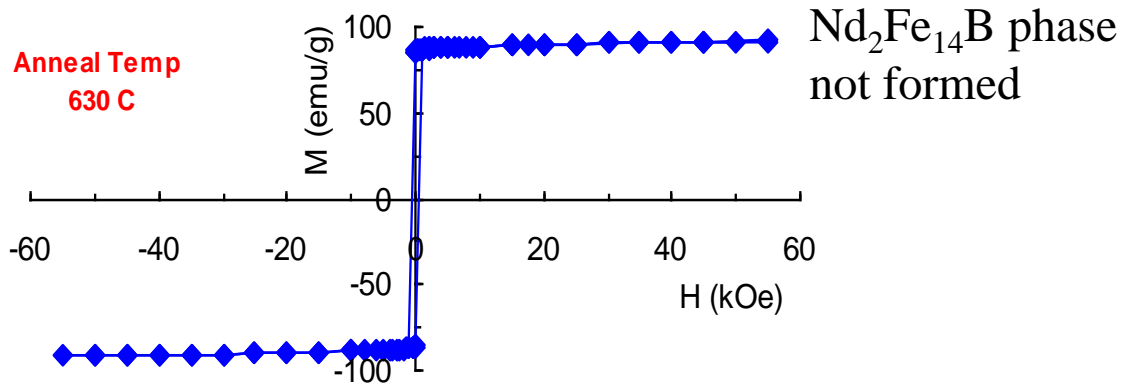
Large interface area
→ NdFeB and Fe coupled.



grain size is 20 – 70 nm.



Exchange coupling (Hf/NdFeB/Hf/Si(110))



From previous work

Best buffer layers: Nb, Mo

Sample thickness: 180 or 540 nm → largest H_c , MH_{max}

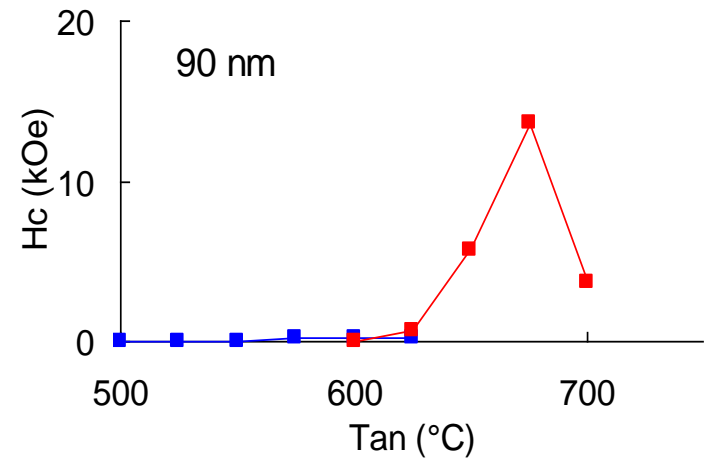
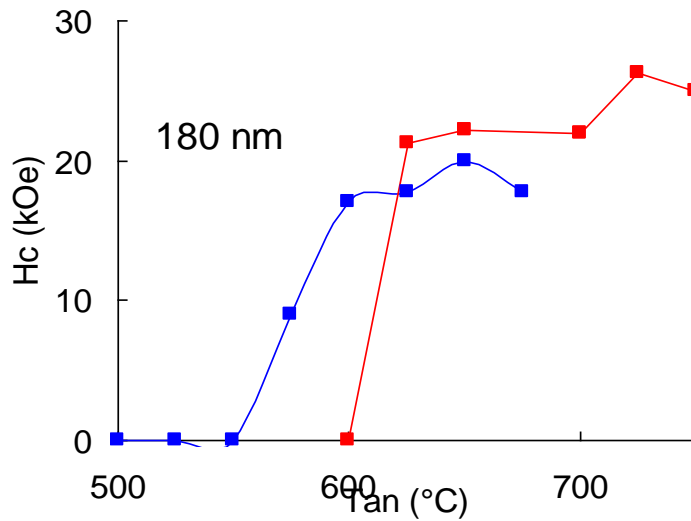
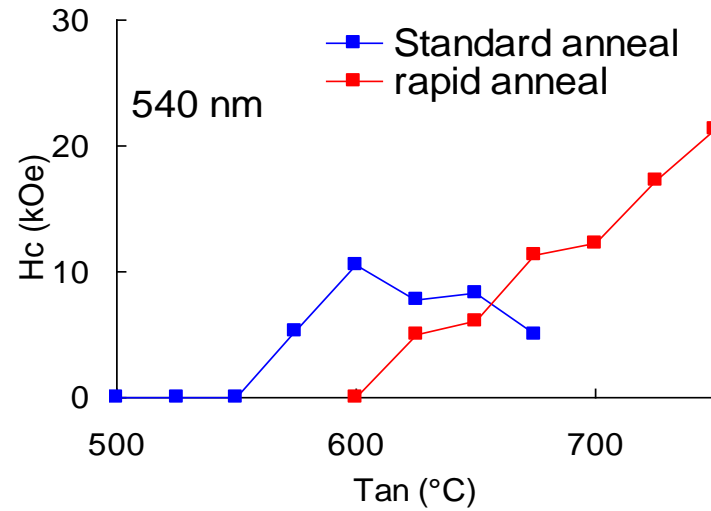
Rapid anneal: larger H_c , MH_{max}

Notes:

The Fe/Nd ratio was determined by PIXE,
7 is stoichiometric $Nd_2Fe_{14}B$

The Nd/B ratio was determined by ICP
mass spectroscopy and is 1.8.

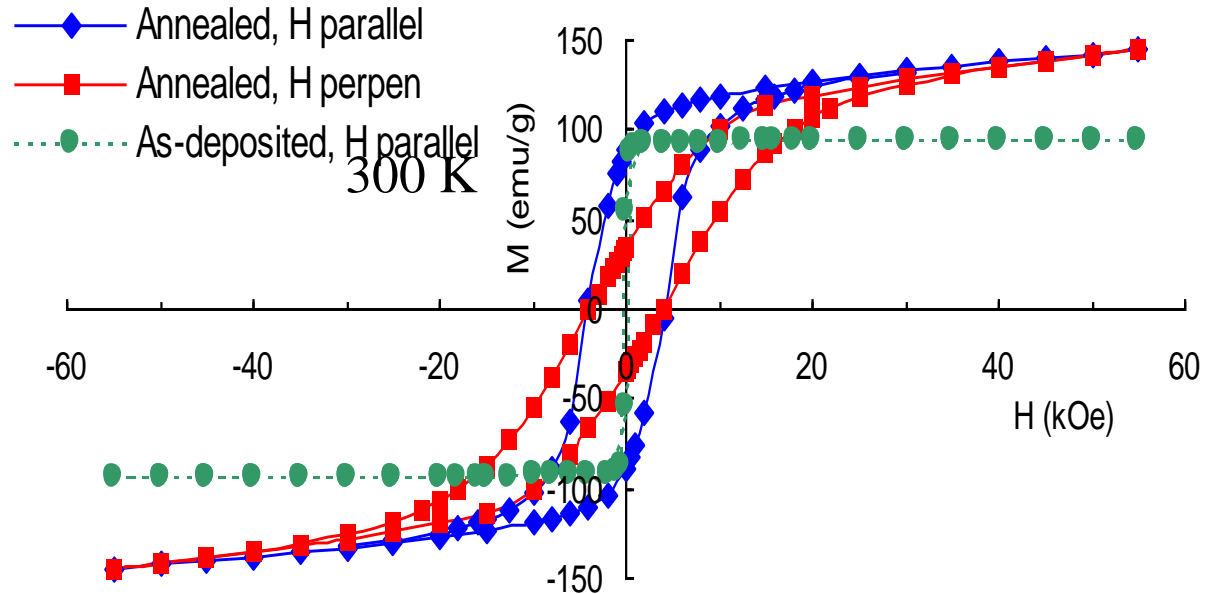
Post anneal: Standard (vacuum) anneal, 20 mins.
Rapid anneal, flowing N, 30 seconds.



[Jiang, O'Shea, to be published in Jour, Magn. Magn. Mat]

Hysteresis loops for:

Nb/NdFeB(540 nm)/Nb/Si,
Rapid (30 sec) anneal at
625 °C.



No in-plane or perpendicular magnetic anisotropy
apart from demagnetization.

(Quantum Design MPMS5 SQUID magnetometer)

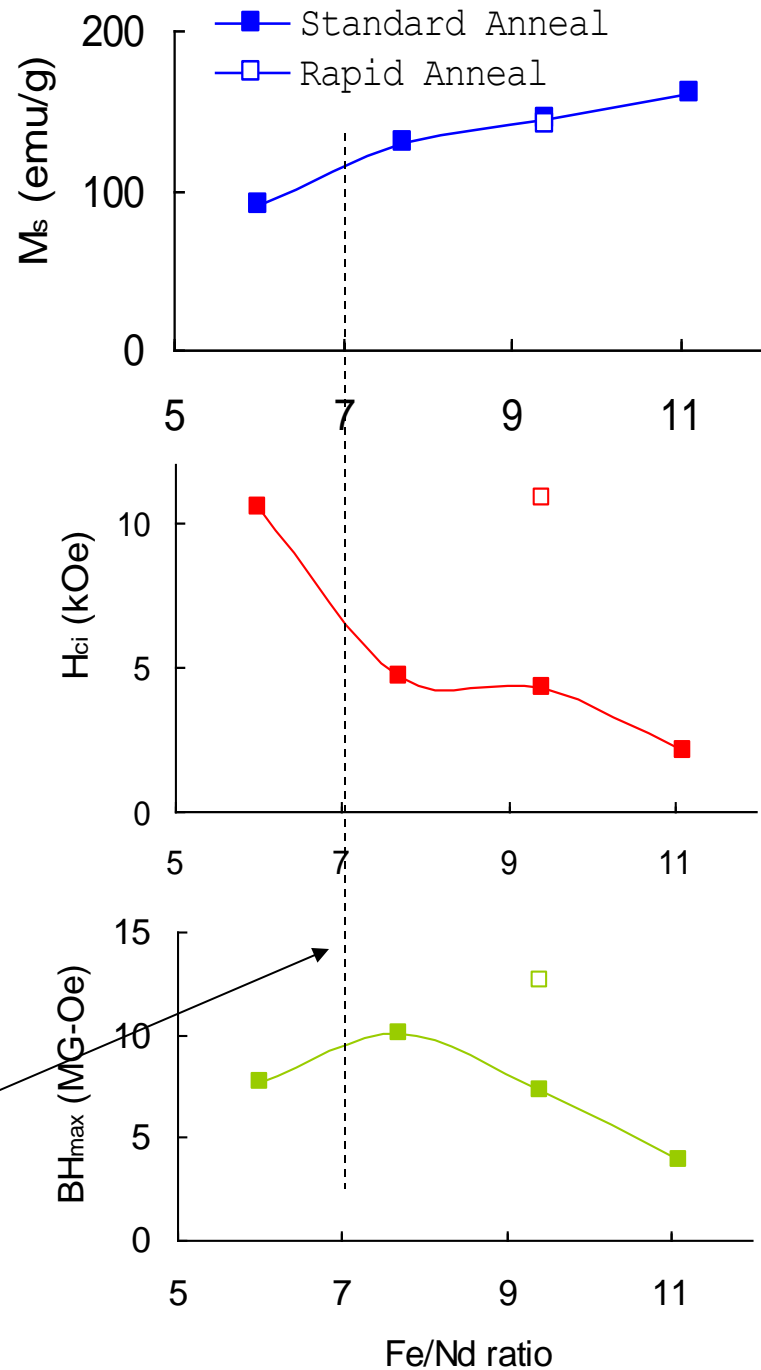
Magnetic Properties as a function of Fe content, $d = 540$ nm, buffer Nb.

Four compositions:

Fe/Nd ratio: 6, 7.7, 9.4, 11.1 (PIXE)

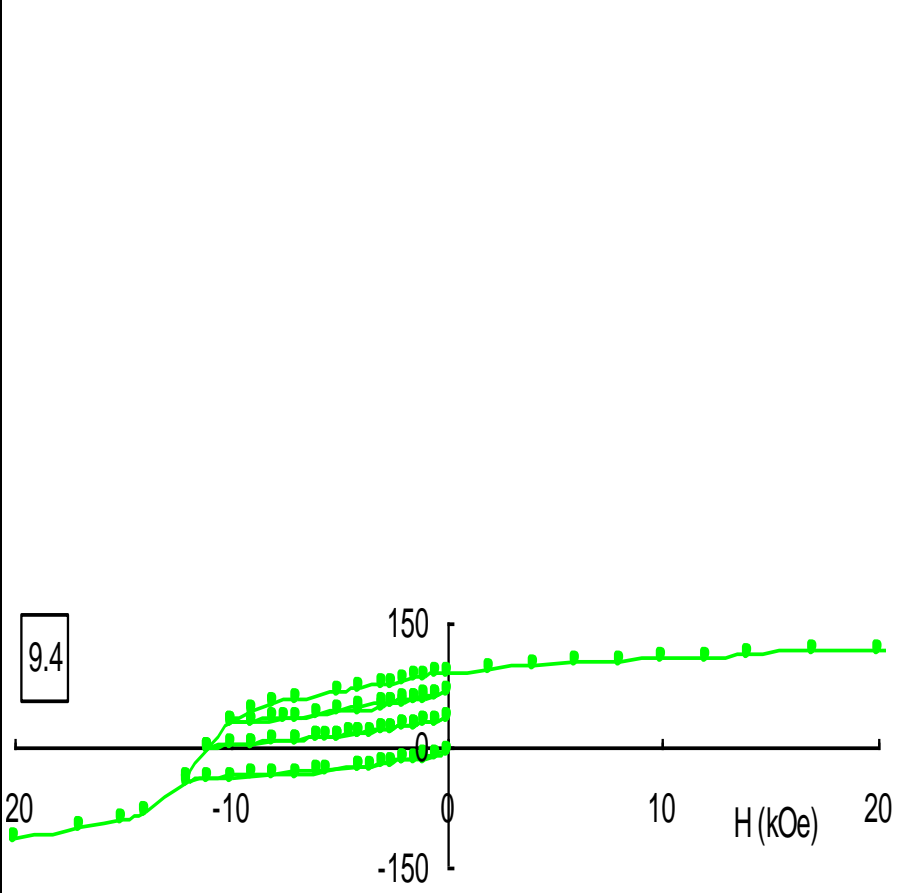
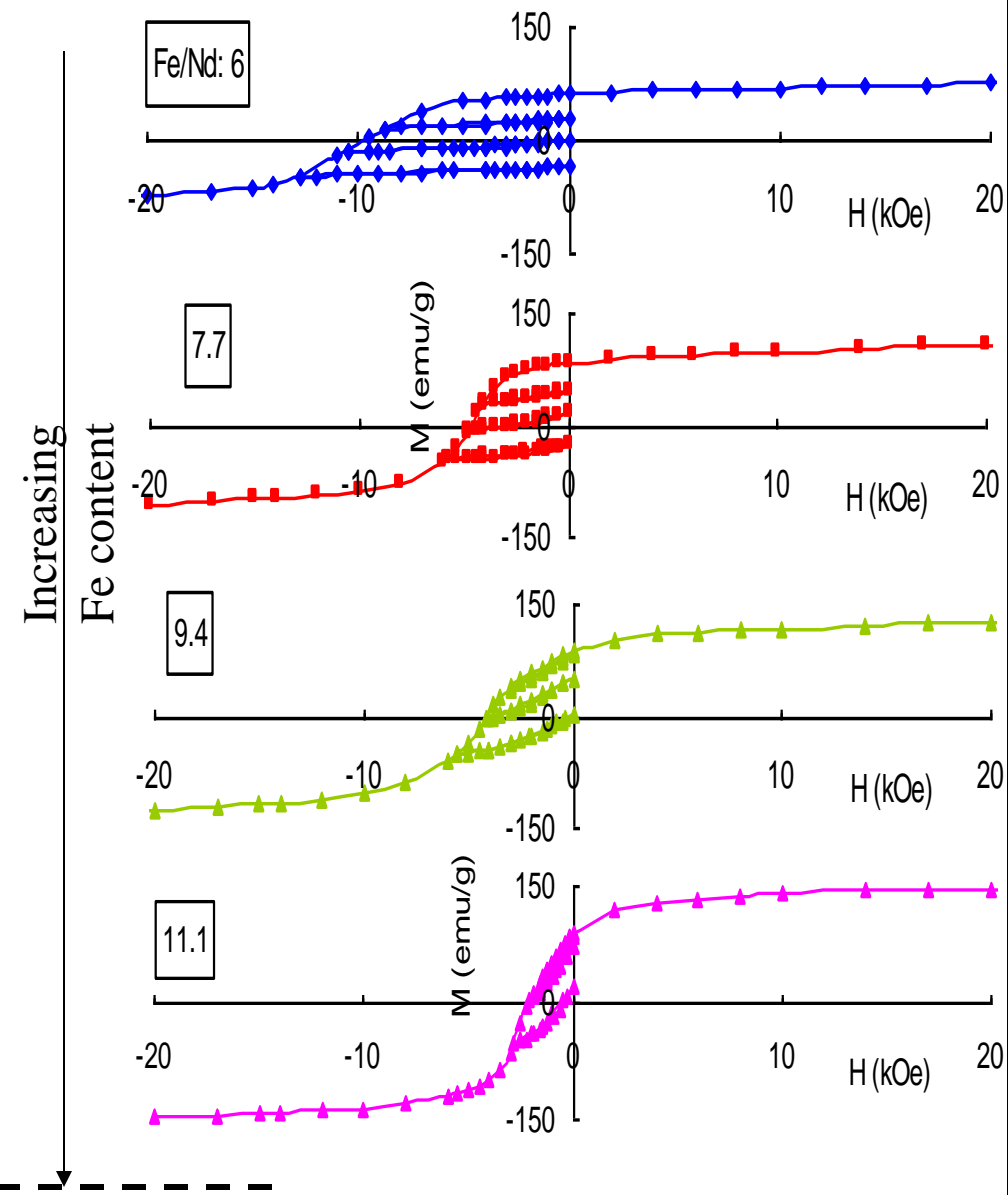
Nd/B ratio: 1.8 (ICP mass spectroscopy)

Stoichiometric
 $\text{Nd}_2\text{Fe}_{14}\text{B}$



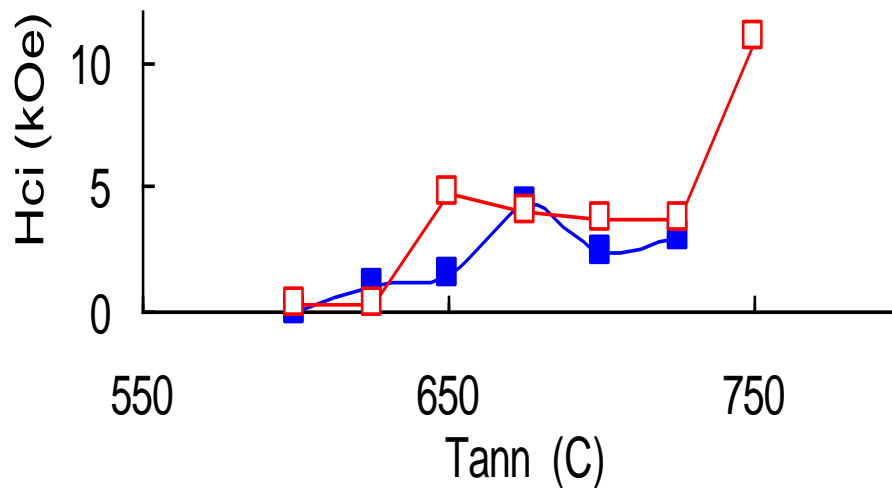
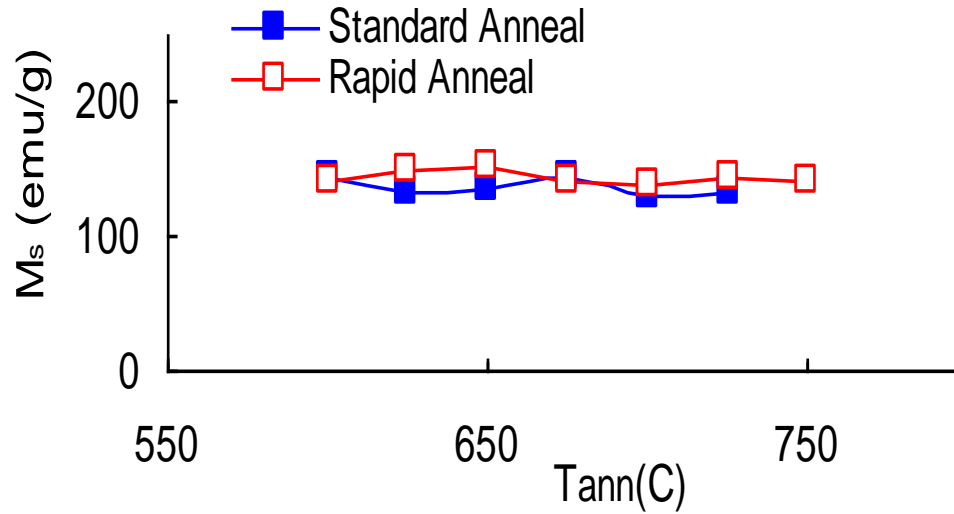
Recoil Magnetization- Standard Anneal

Rapid Anneal



Comparison of a standard and a rapid anneal.

For sample: $d = 540$ nm, Fe/Nd ratio = 9.4



Interactions

Assuming uniform uniaxial single domain particles with no interactions the remanences are related by:

$$M_d(H) = M_R(\infty) - 2M_r(H).$$

M after field:
0 Oe → 55 kOe
→ -H → 0 Oe

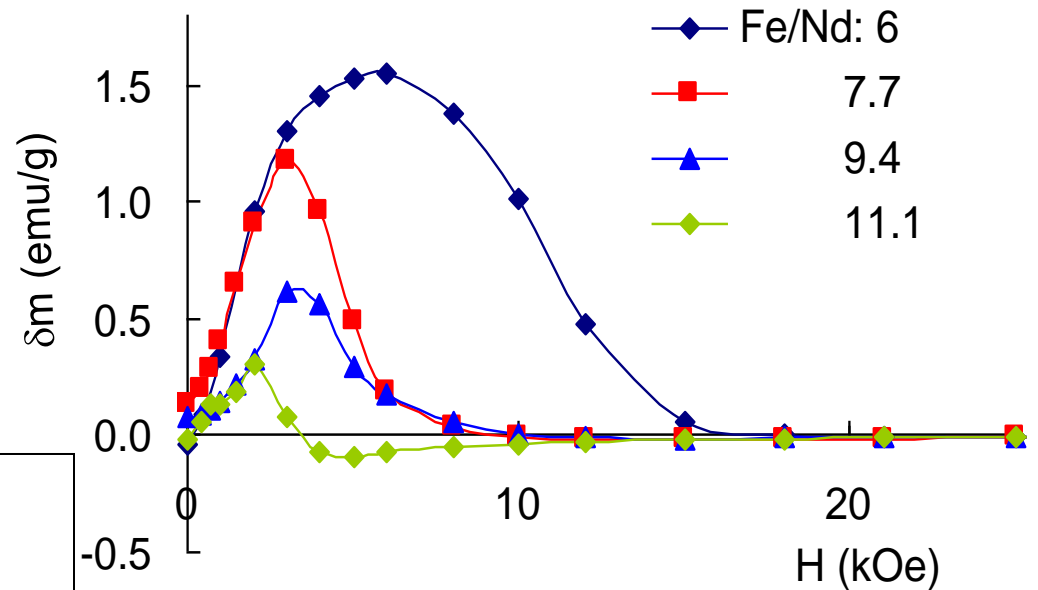
M after field:
0 Oe → 55 kOe → 0 Oe

M after field: 0 Oe → H
→ 0 Oe

If interactions are present this no longer holds and the difference between the left and right side is:

$$\delta m = m_d(H) - (1 - 2m_r(H))$$

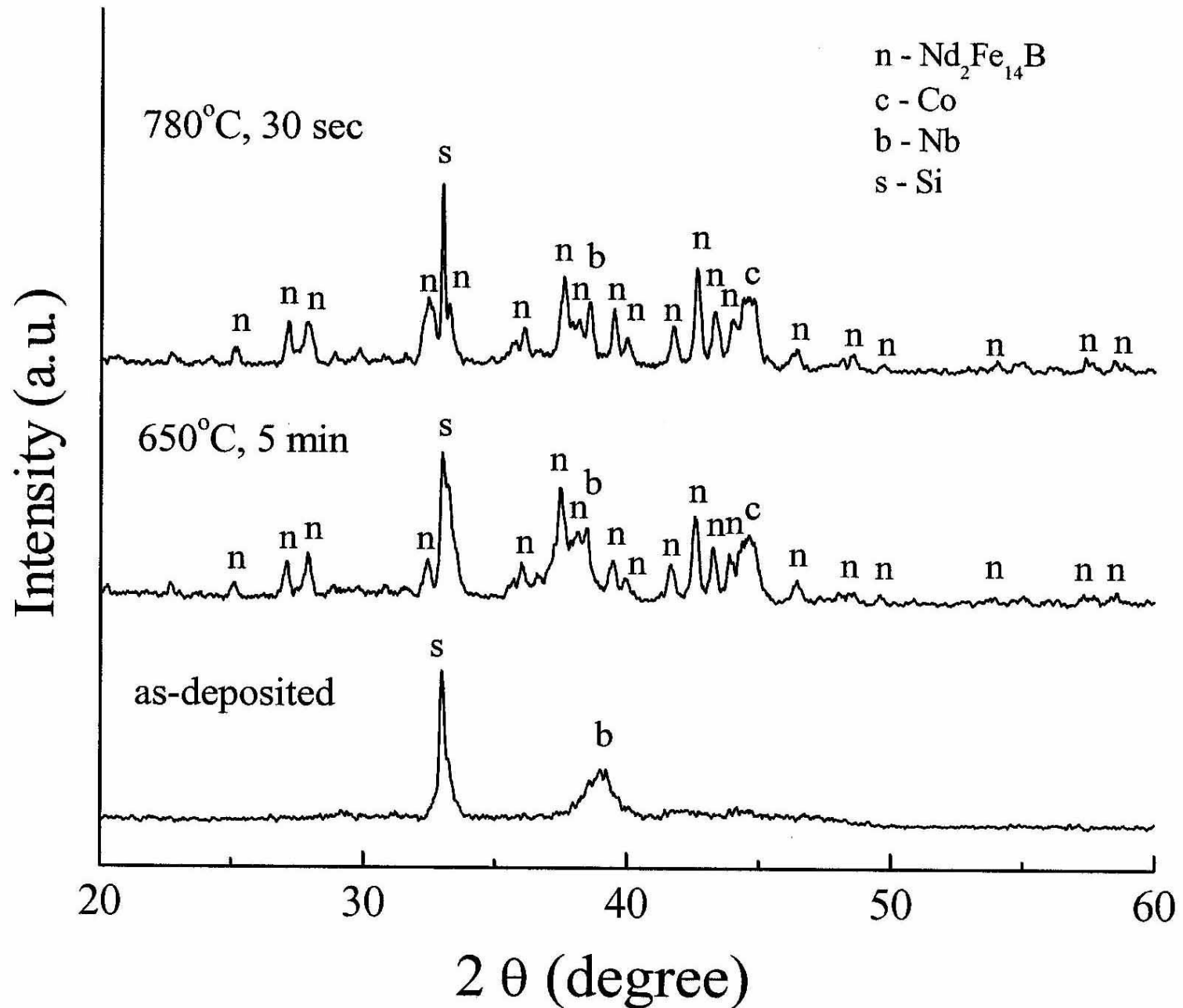
- For samples Fe/Nd=6, 7.7, 9.4, strong positive coupling
- For sample Fe/Nd=11.1, evidence for negative coupling due to magnetostatic interactions



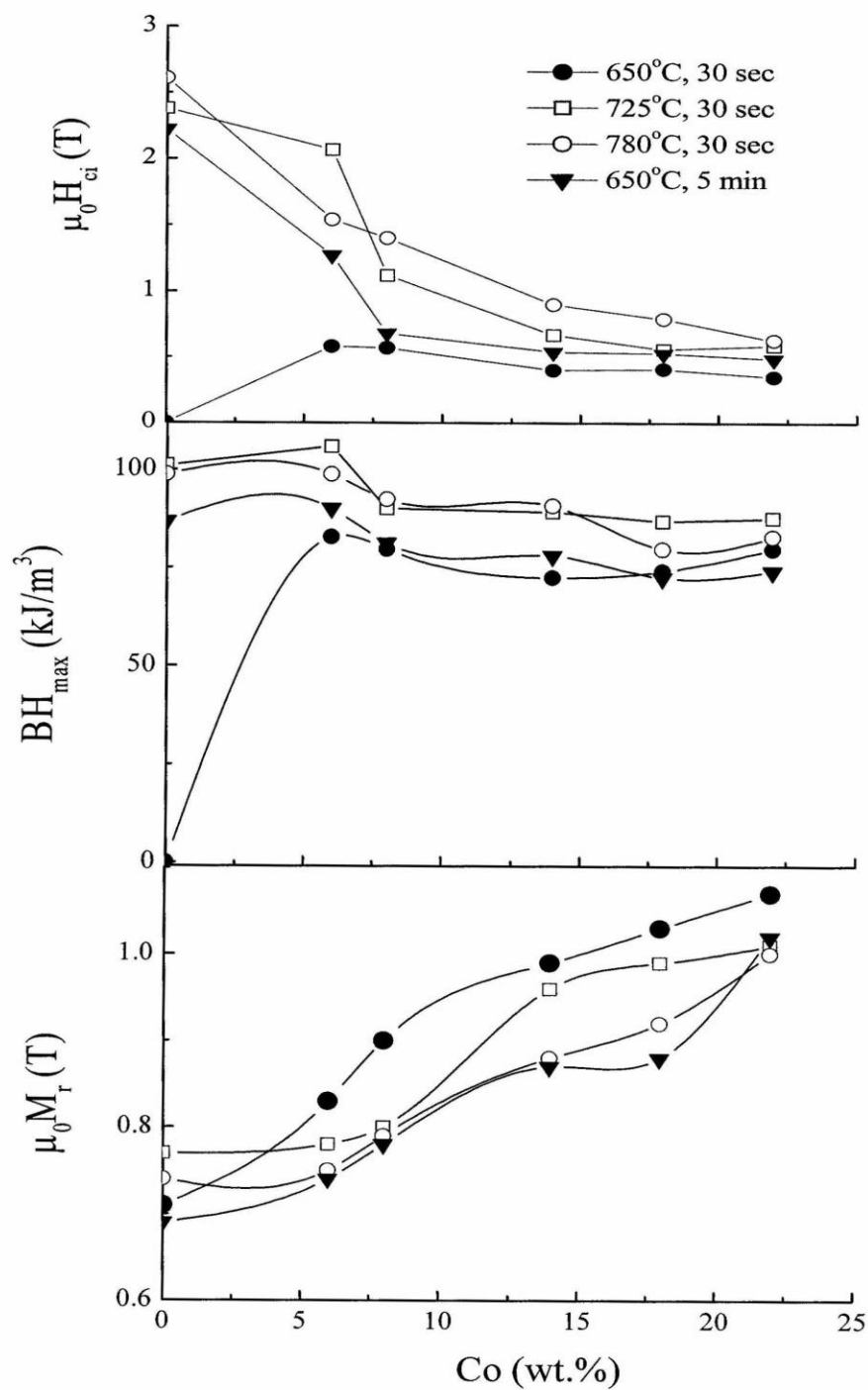
NdFeB/Co –exchange coupled magnets

- Co incorporates a larger moment than $\text{Nd}_2\text{Fe}_{14}\text{B}$
- Co will increase the magnetic ordering temperature
- if Co is incorporated into the $\text{Nd}_2\text{Fe}_{14}\text{B}$ phase $[\text{Nd}_2(\text{FeCo})_{14}\text{B}]$ then the anisotropy of the magnet is lowered.

X-ray diffraction: $\text{Nd}_2\text{Fe}_{14}\text{B}$ +14% Co



H_c , BH_{\max} , $\mu_0 M_r$ as a function of Co content



Structure and magnetic properties

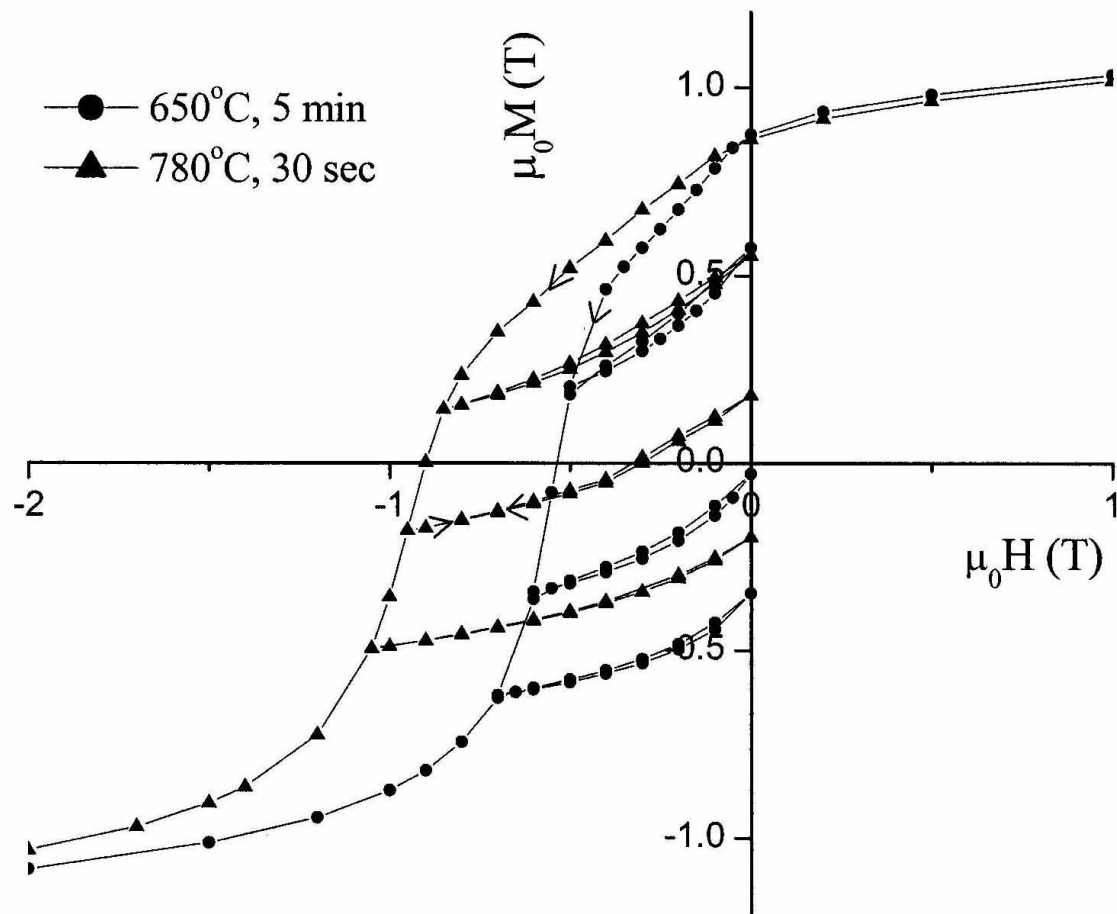
-two selected samples

Grain size

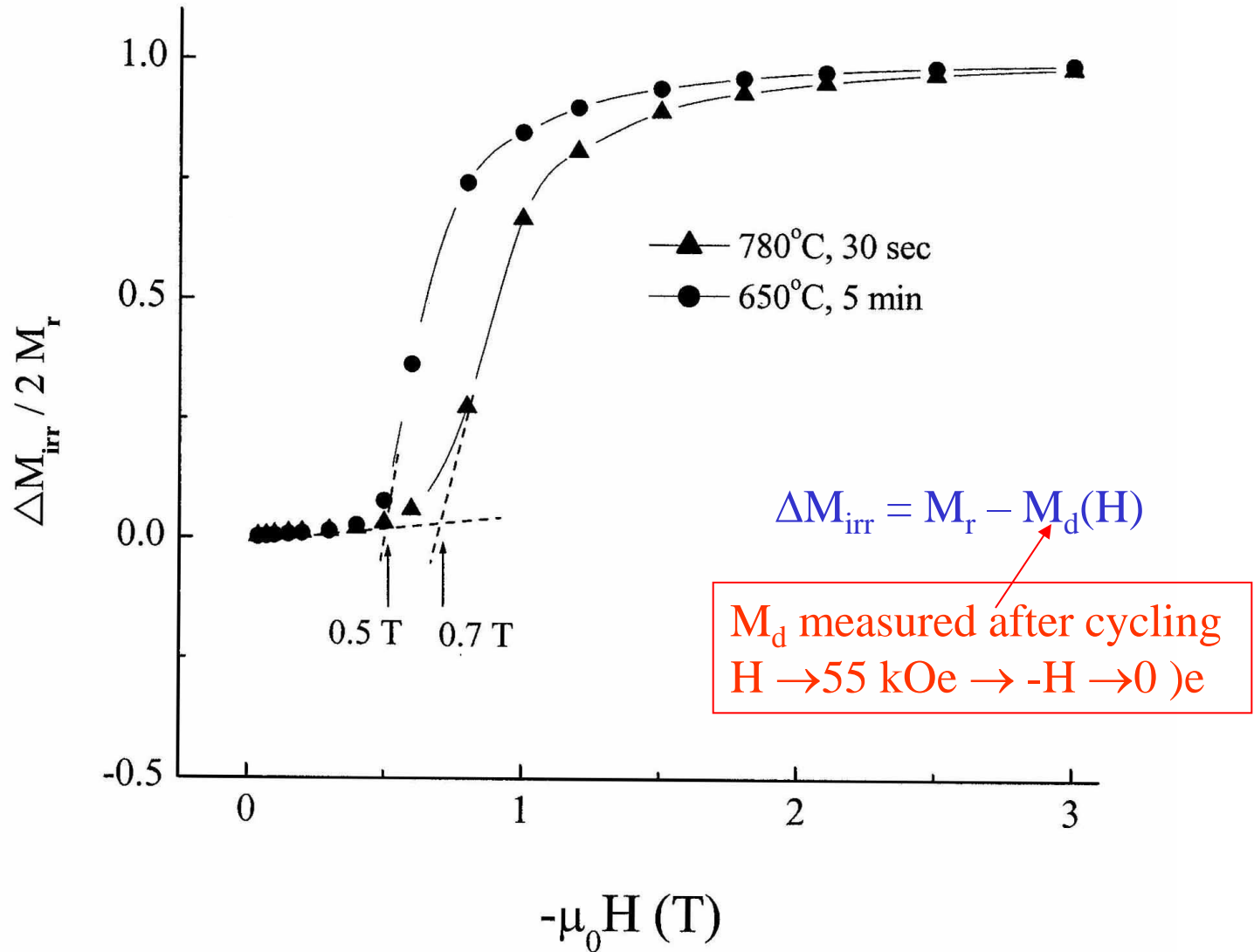


Sample/ T_a (°C)	x (%)	$\mu_0 M_r$ (T) $\pm 1\%$	$\mu_0 H_c$ (T) $\pm 1\%$	BH_{max} (kJ/m ³) $\pm 1\%$	M_r/M_s $\pm 1\%$	Co (nm) $\pm 1n$	$Nd_2Fe_{14}B$ (nm) $\pm 3nm$
650/ 5 mins	14	0.87	0.54	78.0	0.67	^m 15	31
780/ 30 sec	14	0.88	0.9	90.1	0.67	15	29

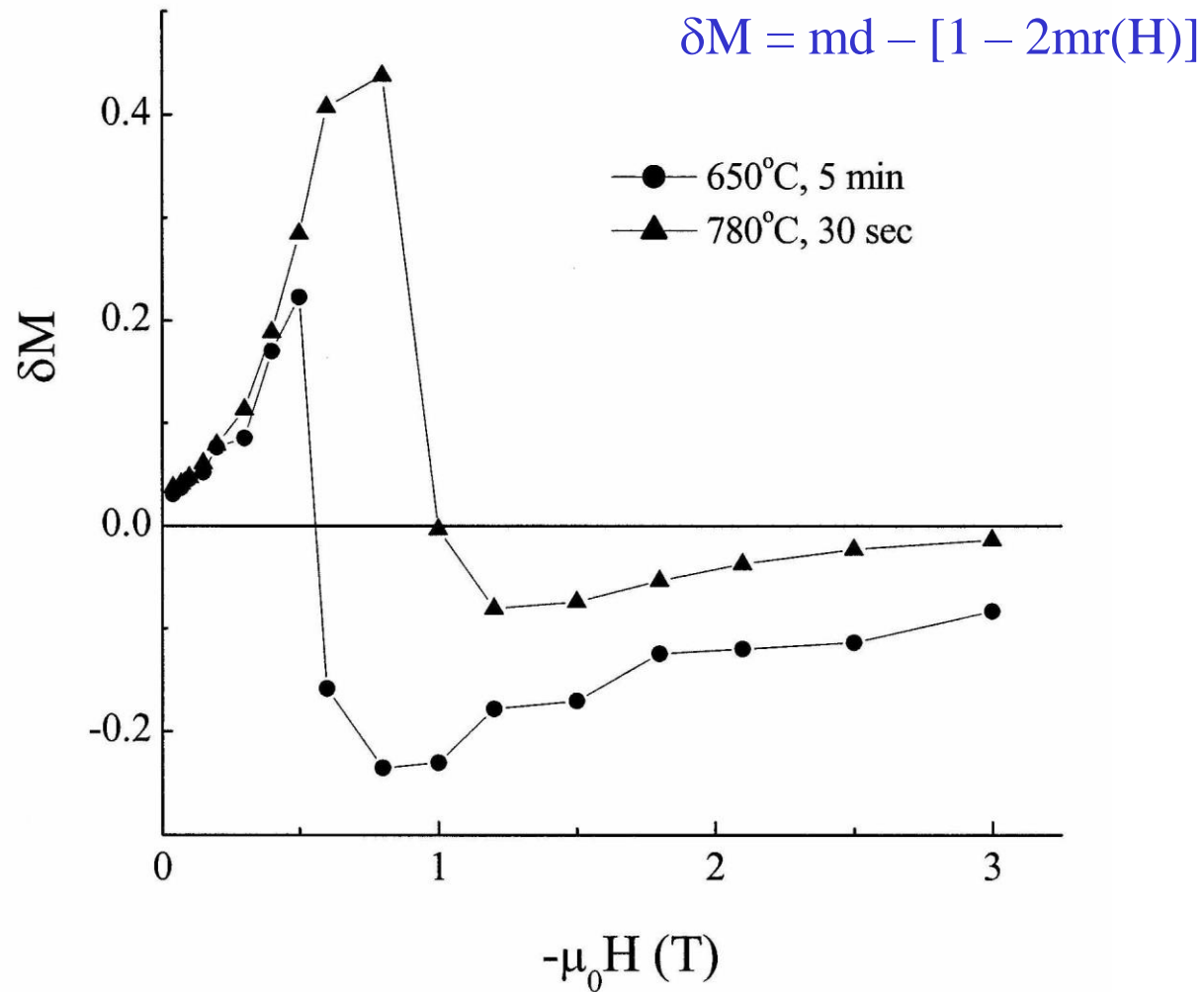
Hysteresis and recoil magnetization



Irreversible magnetization



Henkel Plot



-grains of rapidly annealed samples have positive inter-grain interactions

Energy product

Largest energy product for NdFeCoB is 106 kJ/m^3 (13.3 MG.Oe)

Found in rapidly annealed sample

(Uniform grain size, strong ferromagnetic interactions)

No other work on thin films to compare to.

For bulk melt-spun: 119 kJ/m^3 [1], 95 kJ/m^3 [2], 80 kJ/m^3 [3],
 100 kJ/m^3 [4], 55.7 kJ/m^3 [5].

After aligning grains ref 5 obtains 229 kJ/m^3 ,

1. H. Chiriac, M. Marinescu, Jour. Appl. Phys 83 (1998)
2. L. H. Lewis and V. Panchanathan, Jour. Magn. Mag. Mater. 196 (1999) 299.
3. Q. Chen, B. M. Ma, B. Lu, M. Q. Huang and D. E. Laughlin, Jour. Appl. Phys. 85 (1999) 5917.
4. J. Bernardi, T. Schrefl, J. Fiddler, Th. Rijks, K. de Kort, V. Archambault, D. Pere, S. David, D. Givord, J. F. O'Sullivan, P. A. I. Smith, J. M. D. Coey, U. Czernik, M. Gronefeld, Jour. Magn. Magn. Mater. 219 (2000) 186.
5. R. W. Gao, D. H. Zhang, W. Li, X. M. Li, J. C. Zhang, Jour. Magn. Mag. Mater. 208 (2000) 239.

Final comments

To date magnets based on Nd-Fe-B discovered two decades ago are the best permanent magnets.

Micro- and nano-structure are important in improving their magnetic properties.

With more control on the precise form of nanostructure it is likely properties can be improved (e.g. larger energy products could be obtained)